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BEARING TYPES

NEEDLE ROLLER BEARINGS

Needle roller bearings are an economical alternative for applications requiring minimal space to carry a given load at a desired speed. Needle roller bearings can be an ideal choice because of their ability to handle a given level of speed and load capacity, yet have the smallest cross section of all roller bearing types.

We offer both metric and inch nominal bearings in popular designs such as: radial caged needle rollers, drawn cup needle roller bearings, machined ring, track rollers, thrust bearings, combined bearings, and drawn cup roller clutches.
Most of these bearing types can be operated directly on a machined shaft of suitable quality, or with a matching inner ring where this requirement cannot be conventionally satisfied.

Radial Needle Roller and Cage Assemblies

Radial needle roller and cage assemblies have a steel cage that provides both inward and outward retention for the needle rollers. The designs provide maximum cage strength consistent with the inherently high load ratings of needle roller bearings. Accurate guidance of the needle rollers by the cage bars allows for operation at high speeds. Also available are needle roller and cage assemblies using molded, one-piece glass-reinforced engineered polymer cages. Needle roller and cage assemblies are manufactured with either one or two rows of needle rollers.

Drawn Cup Bearings

The outer ring in the form of a cup is accurately drawn and no subsequent machining is performed to build the outer raceway. Drawn cup needle roller bearings are available in open ends or single, closed-end designs. They also are available with one or two integral seals. Other options include a single lubricating hole and matching inner ring.

Heavy-Duty Needle Roller Bearings

These bearings are available in a wide range of inch and metric sizes plus an array of design features including: integral seals, side flanges (or separate end washers), inner rings, oil holes and single or double caged sets (or full complement) of rollers.

Track Rollers

Track rollers listed in this catalog are designed with outer rings of large radial cross section to withstand heavy rolling and shock loads on track-type or cam-controlled equipment. The outside diameters of the outer rings are either profiled or cylindrical. Profiled track rollers are designed to alleviate uneven bearing loading resulting from deflection, bending or misalignment in mounting. Stud-type track rollers are available with or without lip contact seals, or with shields. Yoke-type track rollers are designed for straddle mounting. Each yoke-type is available with either radial needle roller and cage assemblies, or with a single (or double) full complement row of cylindrical or needle rollers.

Thrust Bearing Assemblies And Washers

Thrust needle roller and cage assemblies are available in a variety of inch or metric sizes. All types have very small cross sections. If the back up surfaces cannot be used as raceways, hardened washers are available. Thrust bearings are available with needle rollers or heavier cylindrical rollers for high load-carrying capacity.

Combined (Radial and Thrust) Bearings

Combined bearings consist of a radial bearing (needle roller bearing) and a thrust bearing (ball or roller bearing). Some combined bearings are constructed similar to drawn cups, but with an added thrust bearing component. Like other needle roller bearings, these combined bearings can be matched with an optional inner ring or thrust washer as the opposing raceway.

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NEEDLE ROLLER BEARING SELECTION

Because of the possible combinations of roller complement orientation, bearing cross section thickness and raceway construction needle roller bearings should be given extra consideration for roller bearing applications selection. The table below should be used as a general guideline for the application of needle roller bearings.

Table A-1. Needle roller bearing capability comparison based on suitable oil lubrication

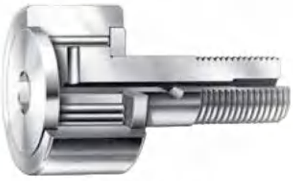
Bearing type/ design capability	Radial needle roller and cage assembly	Drawn cup needle roller bearing caged	Drawn cup roller bearing full complement	Needle roller bearing and inner ring	Track roller	Thrust needle roller and cage assembly	Needle rollers	Combination bearing radial/thrust
Radial load	High	Moderate	High	High	Moderate	None	Very high	High
Axial load	None	None	None	None	Low	Very high	None	High
Limiting speed	Very high	High	Moderate	Very high	Moderate	High	Moderate	Moderate
Slope tolerance	Moderate	Moderate	Very low	Moderate	Moderate(1)	Low	Very low	Low
Grease life	High	High	Low	High	Moderate	Low	Low	Low
Friction	Very low	Very low	Moderate	Very low	Low(2)	Low	Moderate	Moderate
Precision	Very high	Moderate	Moderate	High	High	High	Very high	High
Cross section	Very low	Low	Low	Moderate	High	Very low	Very low	High
Cost	Low	Low	Low	High	High	Moderate	Very low	Very high

(1) "Moderate" for full complement track rollers
(2) "Low" for full complement track rollers


Radial needle roller and cage assembly


Drawn cup needle roller


Heavy-duty needle roller


Track roller


Thrust needle roller and cage assembly


Combined radial/thrust


Drawn cup roller clutch

BEARING REACTIONS, EQUIVALENT LOADS AND BEARING LIFE

DEFINITION OF LOAD RATINGS

Basic Dynamic Load Rating

The "basic dynamic load rating" (Cr) for a radial roller bearing is that calculated, constant, radial load, which a group of apparently identical bearings with stationary outer ring can theoretically endure for a rating life of one million revolutions of the inner ring. For a thrust roller bearing (Ca) is that calculated, constant, centric thrust load, which a group of apparently identical bearings can theoretically endure for a rating life of one million revolutions of one of the bearing washers. The basic dynamic load rating is a reference value only, the base value of one million revolutions has been chosen for ease of calculation. Since applied loading as great as the basic dynamic load tends to cause local plastic deformation of the rolling surfaces, it is not anticipated that such heavy loading would normally be applied.

Basic Static Load Rating

Basic static load rating for a radial roller bearing suitably manufactured from a good quality hardened alloy steel, the static radial load rating (C_{or}) is that uniformly distributed static radial bearing load, which produces a maximum contact stress of 4000 megapascals (580,000 psi) acting at the center of contact of the most heavily loaded rolling element. The static axial load rating (C_{oa}) is that uniformly distributed static centric axial load, which produces a maximum contact stress of 4000 megapascals (580,000 psi) acting at the center of contact of each rolling element.

Note: For a contact stress of 4000 megapascals (580,000 psi) a total permanent deformation of roller and raceway occurs, which is appoximately 0.0001 of the roller diameter.

EQUIVALENT DYNAMIC RADIAL BEARING LOADS (P_R)

To calculate the L_{10} life, it is necessary to calculate a dynamic equivalent radial load, designated by P_r. The dynamic equivalent radial load is defined as a single radial load that, if applied to the bearing, will result in the same life as the combined loading under which the bearing operates.

$$P_r = XF_r + YF_a$$

Where:

- L_{10} = Basic rating life
- P_r = Dynamic equivalent radial load
- F_r = Applied radial load
- F_a = Applied axial load
- X = Radial load factor
- Y = Axial load factor

Radial needle roller bearings are designed to carry radial load with zero thrust load under normal conditions. With the thrust load equal to zero, equivalent radial load (P_r) is equal to the design radial load (F_r). Your representative should be consulted on any applications where thrust load is involved (as the resulting increase in internal friction may require cooling to prevent increased operating temperatures).

STATIC RADIAL AND/OR AXIAL EQUIVALENT LOADS

The static equivalent radial and/or axial loading is dependent on the bearing type selected. For bearings designed to accommodate only radial or thrust loading, the static equivalent load is equal to the applied load.

For all bearings, the maximum contact stress can be approximated using the static equivalent load and the static rating.

For roller bearings:

$$\sigma_0 = 4000 \times \left(\frac{P_0}{C_0}\right)^{1/2} \text{ MPa}$$

$$\sigma_0 = 580 \times \left(\frac{P_0}{C_0}\right)^{1/2} \text{ ksi}$$

Because radial needle roller bearings are not designed to accept thrust loading, their equation to determine static radial equivalent load is:

$$P_{0r} = F_r$$

Thrust needle roller bearings are not designed to accept radial loading, so their equation to determine static thrust equivalent load is:

$$P_{0a} = F_a$$

The determination of the static load safety factor (f_0) serves to ascertain that a bearing with adequate static load rating has been selected.

$$f_0 = \frac{C_0}{P_0}$$

Where:

- f_0 = Static load safety factor
- C_0 = Basic static load rating (kN or lbf)
- P_0 = Maximum applied static load (kN or lbf)

f_0 is a safety factor against permanent deformation of the contact areas of the rolling elements and raceways. Higher f_0 values are required for particulary smooth operation. The following values are generally suggested.

- f_0 = 1.5 ... 3.0 for smooth operation
- f_0 = 1.0 ... 2.0 for less smooth operation

For drawn cup needle roller bearings, f_0 should be ≥3.

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MINIMUM BEARING LOAD

Slippage can occur if loads are too light and, if accompanied by inadequate lubrication, can cause damage to the bearings. The minimum load for bearings with cage is $P_r/C_r = 0.02$, for full-complement bearings $P_r/C_r = 0.04$ (P_r is the dynamic load and C_r is the basic dynamic load rating).

Thrust needle roller bearings also have an added design requirement such that the minimum thrust load is satisfied to prevent the rollers from skidding on the raceway. The equation for the thrust loading force is different for needle rollers versus cylindrical rollers as noted:

(Needle rollers) $F_{a\ min.} = C_{0a}/2200$ kN
(Cylindrical rollers) $F_{a\ min.} = 0.1C_{0a}/2200$ kN

MAXIMUM BEARING LOAD

The load/life relationship is applicable to a wide range of bearing loads. However, high loading may cause stress concentrations in the roller-raceway contacts. Therefore, for most applications, the maximum applied load should not be greater than one-third of the basic dynamic load rating [$P \leq C/3$] in order for the basic rating life calculation to be valid.

MEAN DYNAMIC EQUIVALENT LOAD

When load magnitude or direction varies, it is necessary to calculate the mean dynamic equivalent load, which provides the same length of bearing service life as that under the actual load fluctuation. If the load and the rotational speed change in levels, as shown in Fig. A-1, the following equation can be used to calculate the mean dynamic equivalent load.

$$P_m = \sqrt[10/3]{\frac{P_1^{10/3} n_1 t_1 + P_2^{10/3} n_2 t_2 + \cdots\cdots + P_n^{10/3} n_n t_n}{n_1 t_1 + n_2 t_2 + \cdots\cdots\cdots + n_n t_n}}$$

In this equation,

P_m : Mean dynamic equivalent load N
P_1 : The load applied at rotational speed n_1 and for t_1 hours N
⋮
P_n : The load applied at rotational speed n_n and for t_n hours N

What's more, the following equation can be used to calculate the mean rotational speed n_m.

$$n_m = \frac{n_1 t_1 + n_2 t_2 + \cdots\cdots + n_n t_n}{t_1 + t_2 + \cdots\cdots\cdots\cdots t_n}$$

When the load changes steadily, as shown in Fig. A-2, the following equation can be used to calculate an approximation of the mean dynamic equivalent load.

$$P_m = \frac{P_{min.} + 2\,P_{max.}}{3}$$

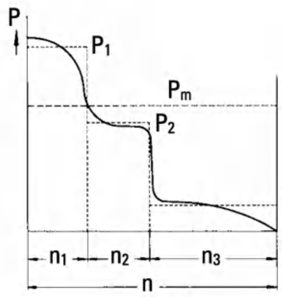


Fig. A-1

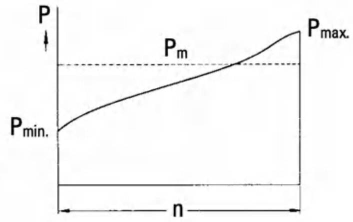


Fig. A-2

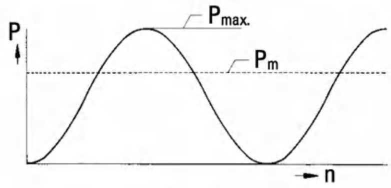


Fig. A-3

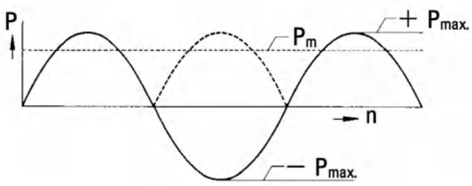


Fig. A-4

In this equation,

$P_{min.}$: The minimum dynamic equivalent load N
$P_{max.}$: The maximum dynamic equivalent load N

When the load changes like a sine wave between 0 and P_{max}, as shown in Fig. A-3, the following equation can be used to calculate an approximation of the mean dynamic equivalent load.

$$P_m \fallingdotseq 0.68\,P_{max.}$$

When the load changes between 0 and $P_{max.}$ in only the upper half of the sine wave, as shown in Fig. A-4, the following equation can be used to calculate an approximation of the mean dynamic equivalent load.

$$P_m \fallingdotseq 0.75\,P_{max.}$$

BEARING LIFE

Even if rolling bearings are rotated under ideal conditions, contact stress is continuously and repeatedly applied to the raceway surfaces of inner and outer rings or rolling contact surfaces of rolling elements, and material flakes from the raceway surfaces and rolling contact surfaces due to fatigue of material. The total number of bearing rotations (or total operating period at a constant speed) until flaking occurs is regarded as the bearing service life.

Even if bearings of the same dimensions, structure, material, and processing method are operated under the same rotating conditions, their service lives are considerably varied.

Since this phenomenon results from fatigue distribution in bearing materials themselves, differences in bearing service life should be statistically considered. When a group of identical bearings are rotated under the same conditions, the total number of revolutions until 90 % of the bearings are left without flaking (i.e. a service life of 90 % reliability) is defined as the basic rating life. Or in operating at a constant speed, it can be expressed by the total number of bearing rotations.

In practical service, however, a bearing fails not only because of fatigue, but other coefficients as well, such as wear, seizure, creep, fretting, brinelling, cracking etc. These bearing failures can be minimized by selecting the proper mounting method and lubricant, as well as the bearing most suitable for the application.

BEARING LIFE EQUATIONS

Basic Rating Life

Generally, the relationship between the basic dynamic load rating, dynamic equivalent load, and basic rating life of needle roller bearings is expressed as follows.

$$L_{10} = \left(\frac{C}{P}\right)^{10/3}$$

Where,

L_{10} :	Basic rating life	10^6 rotations
C :	Basic dynamic load rating	N
P :	Dynamic equivalent load	N

It is common for the life being expressed in terms of time to be useful when the bearing is rotating at a constant speed.

In this situation, the life can be obtained with the following equation.

$$L_{10h} = \left(\frac{C}{P}\right)^{10/3} \frac{10^6}{60n}$$

Where,

L_{10h} :	Basic rating life	h
n :	Rotational speed	min^{-1}

Accordingly, where the dynamic equivalent load is P and rotational speed is n, the following equation can be used to calculate the basic dynamic load rating C, which is required to meet the design life. The bearing size most suitable for a specified purpose can then be selected by referring to the bearing specification table.

$$C = P\left(L_{10h} \times \frac{60n}{10^6}\right)^{3/10}$$

Modified Rating Life

The life of rolling bearings was standardized as a basic rating life in the 1960s, but in actual applications, sometimes the actual life and the basic rating life have been quite different due to the lubrication status and the influence of the usage environment. To make the calculated life closer to the actual life, a corrected rating life has been considered since the 1980s. In this corrected rating life, bearing characteristic factor a_2 (a correction factor for the case in which the characteristics related to the life are changed due to the bearing materials, manufacturing process, and design) and usage condition factor a_3 (a correction factor that takes into account usage conditions that have a direct influence on the bearing life, such as the lubrication) or factor a_{23} formed from the interdependence of these two factors, are considered with the basic rating life. These factors were handled differently by each bearing manufacturer, but they have been standardized as a modified rating life in **ISO 281** in 2007. In 2013, **JIS B 1518** (dynamic load ratings and rating life) was amended to conform to the **ISO**.

The basic rating life (L_{10}) shown in equation is the (fatigue) life with a dependability of 90 % under normal usage conditions for rolling bearings that have standard factors such as internal design, materials, and manufacturing quality. **JIS B 1518**:2013 specifies a calculation method based on **ISO 281**:2007. To calculate accurate bearing life under a variety of operating conditions, it is necessary to consider elements such as the effect of changes in factors that can be anticipated when using different reliabilities and system approaches, and interactions between factors. Therefore, the specified calculation method considers additional stress due to the lubrication status, lubricant contamination, and fatigue load limit C_u (refer to p. A-9) on the inside of the bearing. The life that uses this life modification factor a_{ISO}, which considers the above factors, is called modified rating life L_{nm} and is calculated with the following equation.

$$L_{nm} = a_1 \, a_{ISO} \, L_{10}$$

In this equation,

L_{nm} : Modified rating life — 10^6 rotations

(This rating life has been modified for one of or a combination of the following: reliability of 90 % or higher, fatigue load limit, special bearing characteristics, lubrication contamination, and special operating conditions.)

L_{10} : Basic rating life — 10^6 rotations (reliability: 90 %)

a_1 : Life modification factor for reliability ··············· Refer to section (1)

a_{ISO} : Life modification factor ··············· Refer to section (2)

[Remark]
When bearing dimensions are to be selected given L_{nm} greater than 90 % in reliability, the strength of shaft and housing must be considered.

(1) Life modification factor for reliability a_1

The term “reliability” is defined as “for a group of apparently identical rolling bearings, operating under the same conditions, the percentage of the group that is expected to attain or exceed a specified life” in **ISO 281**:2007. Values of a_1 used to calculate a modified rating life with a reliability of 90 % or higher (a failure probability of 10 % or less) are shown in Table A-2.

Table A-2. Life modification factor for reliability a_1

Reliability, %	L_{nm}	a_1
90	L_{10m}	1
95	L_{5m}	0.64
96	L_{4m}	0.55
97	L_{3m}	0.47
98	L_{2m}	0.37
99	L_{1m}	0.25
99.2	$L_{0.8m}$	0.22
99.4	$L_{0.6m}$	0.19
99.6	$L_{0.4m}$	0.16
99.8	$L_{0.2m}$	0.12
99.9	$L_{0.1m}$	0.093
99.92	$L_{0.08m}$	0.087
99.94	$L_{0.06m}$	0.080
99.95	$L_{0.05m}$	0.077

(Citation from **JIS B 1518**:2013)

(2) Life modification factor a_{ISO}

a) System approach

The various influences on bearing life are dependent on each other. The system approach of calculating the modified life has been evaluated as a practical method for determining life modification factor a_{ISO} (ref. Fig. A-5). Life modification factor a_{ISO} is calculated with the following equation. A diagram is available for each bearing type (radial ball bearings, radial roller bearings, thrust ball bearings, and thrust roller bearings). (Each diagram (Figs. A-6 to A-9) is a citation from **JIS B 1518**:2013.)

Note that in practical use, this is set so that life modification factor $a_{ISO} \leq 50$.

$$a_{ISO} = f\left(\frac{e_c C_u}{P}, \kappa\right)$$

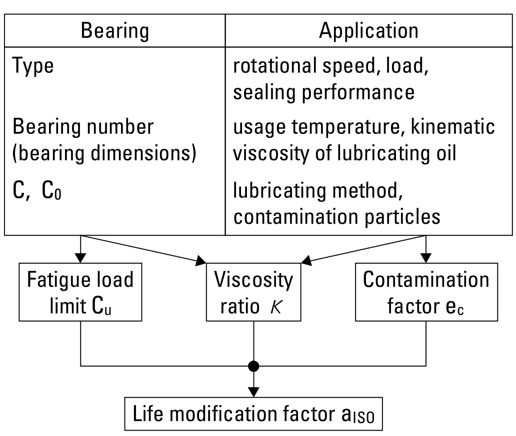


Fig. A-5. System approach

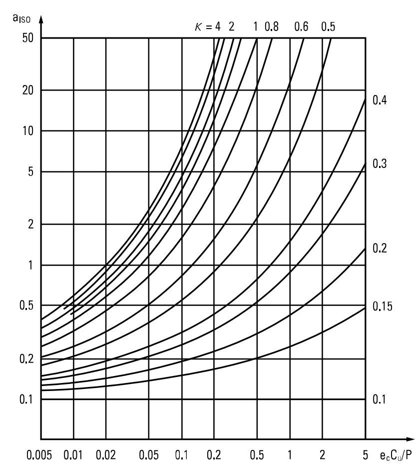


Fig. A-6. Life modification factor a_{ISO} (Radial ball bearings)

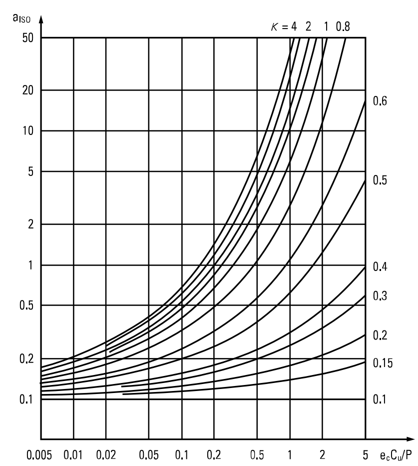


Fig. A-7. Life modification factor a_{ISO} (Radial roller bearings)

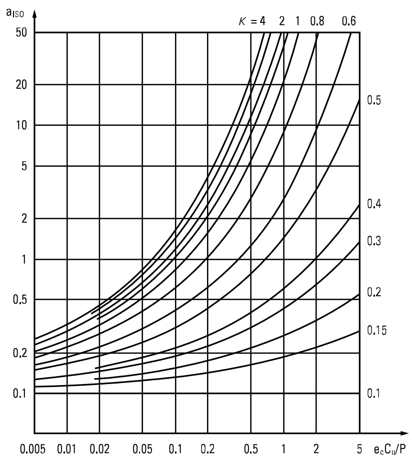


Fig. A-8. Life modification factor a_{ISO} (Thrust ball bearings)

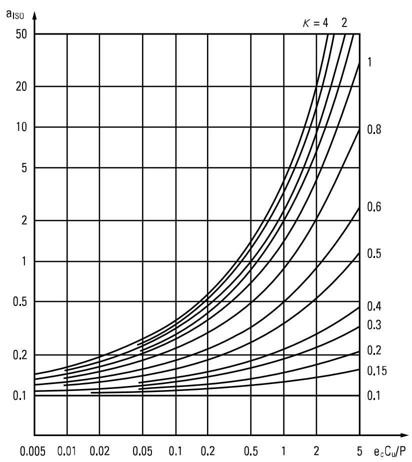


Fig. A-9. Life modification factor a_{ISO} (Thrust roller bearings)

(Figs. A-6 to A-9. Citation from **JIS B 1518**:2013)

b) Fatigue load limit C_u

For regulated steel materials or alloy steel that has equivalent quality, the fatigue life is unlimited so long as the load condition does not exceed a certain value and so long as the lubrication conditions, lubrication cleanliness class, and other operating conditions are favorable. For general high-quality materials and bearings with high manufacturing quality, the fatigue stress limit is reached at a contact stress of approximately 1.5 GPa between the raceway and rolling elements. If one or both of the material quality and manufacturing quality are low, the fatigue stress limit will also be low.

The term "fatigue load limit" C_u is defined as "bearing load under which the fatigue stress limit is just reached in the most heavily loaded raceway contact" in **ISO 281**:2007. and is affected by factors such as the bearing type, size, and material.

For details on the fatigue load limits of special bearings and other bearings not listed in this catalog, contact JTEKT.

c) Contamination factor e_C

If solid particles in the contaminated lubricant are caught between the raceway and the rolling elements, indentations may form on one or both of the raceway and the rolling elements. These indentations will lead to localized increases in stress, which will decrease the life. This decrease in life attributable to the contamination of the lubricant can be calculated from the contamination level as contamination factor e_C.

D_{pw} shown in Table A-3 is the pitch diameter of ball/roller set, which is expressed simply as D_{pw} = (D + d)/2. (D: Outside diameter, d: Bore diameter)

For information such as details on special lubricating conditions or detailed investigations, contact JTEKT.

Table A-3. Values of contamination factor e_C

Contamination level	e_C	
	D_{pw} < 100 mm	$D_{pw} \geq$ 100 mm
Extremely high cleanliness: The size of the particles is approximately equal to the thickness of the lubricant oil film, this is found in laboratory-level environments.	1	1
High cleanliness: The oil has been filtered by an extremely fine filter, this is found with standard grease-packed bearings and sealed bearings.	0.8 to 0.6	0.9 to 0.8
Standard cleanliness: The oil has been filtered by a fine filter, this is found with standard grease-packed bearings and shielded bearings.	0.6 to 0.5	0.8 to 0.6
Minimal contamination: The lubricant is slightly contaminated.	0.5 to 0.3	0.6 to 0.4
Normal contamination: This is found when no seal is used and a coarse filter is used in an environment in which wear debris and particles from the surrounding area penetrate into the lubricant.	0.3 to 0.1	0.4 to 0.2
High contamination: This is found when the surrounding environment is considerably contaminated and the bearing sealing is insufficient.	0.1 to 0	0.1 to 0
Extremely high contamination	0	0

(Table A-3. Citation from **JIS B 1518**:2013)

d) Viscosity ratio κ

The lubricant forms an oil film on the roller contact surface, which separates the raceway and the rolling elements. The status of the lubricant oil film is expressed by viscosity ratio κ, the actual kinematic viscosity at the operating temperature ν divided by the reference kinematic viscosity ν_1 as shown in the following equation.

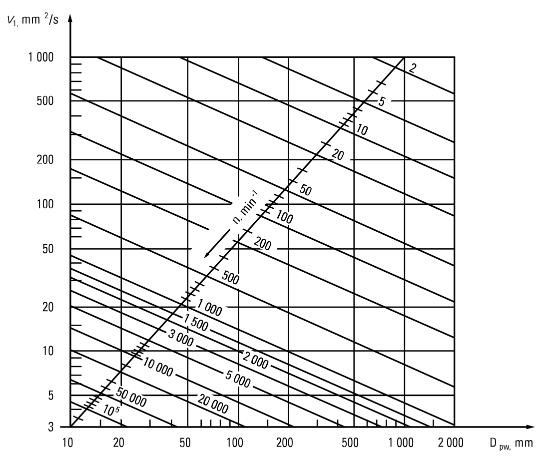
A κ greater than 4, equal to 4, or less than 0.1 is not applicable.

For details on lubricants such as grease and lubricants with extreme pressure additives, contact JTEKT.

$$\kappa = \frac{\nu}{\nu_1}$$

ν : Actual kinematic viscosity at the operating temperature; the viscosity of the lubricant at the operating temperature (refer to Fig. A-14, p. A-22)

ν_1 : Reference kinematic viscosity; determined according to the speed and pitch diameter of ball/roller set D_{pw} of the bearing (ref. Fig. A-10)



(Fig. A-10. Citation from **JIS B 1518**:2013)

Fig. A-10. Reference kinematic viscosity ν_1

Basic Dynamic Load Rating Correction Due to Temperature

During high-temperature operation, the bearing metal hardness deteriorates as the material compositions are altered. As a result, the basic dynamic load rating is diminished. Once altered, material composition does not recover, even if the operating temperature is returned to normal. Therefore, for bearings used in high temperature operations, the basic dynamic load rating must be corrected by multiplying the basic dynamic load rating values specified in the bearing specification table by the temperature coefficient values in Table A-4.

Table A-4. Temperature coefficient values

Bearing temperature, °C	125	150	175	200	250
Temperature coefficient	1	1	0.95	0.90	0.75

Hardness rating factors

Dynamic and static load ratings are based on a minimum raceway hardness equivalent to 58 HRC (HV 653). If the raceway hardness is lower, the effective load ratings will be decreased. The following factors may be used to estimate life when raceway hardness is lower than 58 HRC. Thorough validation is recommended.

Table A-5. Basic dynamic load rating coefficients

Hardness (HRC)	Coefficient
58	1
57	0.94
56	0.89
55	0.85
54	0.80
53	0.75
52	0.68
51	0.60
50	0.50
49	0.44
48	0.40
47	0.37
46	0.34
45	0.31
40	0.20

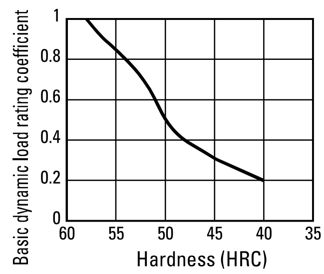


Fig. A-11. Relationship between basic dynamic load rating coefficient and hardness

Table A-6. Basic static load rating coefficients

Hardness (HRC)	Coefficient
58	1
57	0.94
56	0.88
55	0.83
54	0.78
53	0.73
52	0.68
51	0.65
50	0.61
49	0.57
48	0.53
47	0.50
46	0.47
45	0.44
40	0.32

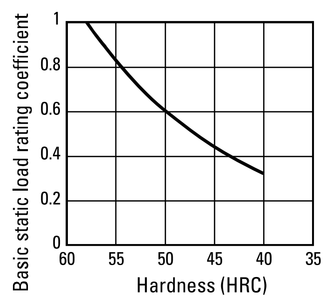


Fig. A-12. Relationship between basic static load rating coefficient and hardness

Service life of bearing system comprising two or more bearings

Even for systems which comprise two or more bearings, if one bearing is damaged, the entire system malfunctions.

Where all bearings used in an application are regarded as one system, the service life of the bearing system can be calculated using the following equation,

$$\frac{1}{L^e} = \frac{1}{L_1{}^e} + \frac{1}{L_2{}^e} + \frac{1}{L_3{}^e} + \cdots\cdots\cdots$$

where :

L : rating life of system

L_1 , L_2 , L_3······ : rating life of each bearing

e : constant

e = 10/9······ball bearing
e = 9/8······roller bearing
The mean value is for a system using both ball and roller bearings.

[Example]

When a shaft is supported by two roller bearings whose service lives are 50 000 hours and 30 000 hours respectively, the rating life of the bearing system supporting this shaft is calculated as follows :

$$\frac{1}{L^{9/8}}=\frac{1}{50\,000^{9/8}}+\frac{1}{30\,000^{9/8}}$$

$$L \fallingdotseq 20\,000 \text{ h}$$

This fact is very important in estimating bearing service life for applications using two or more bearings.

MOUNTING DESIGNS

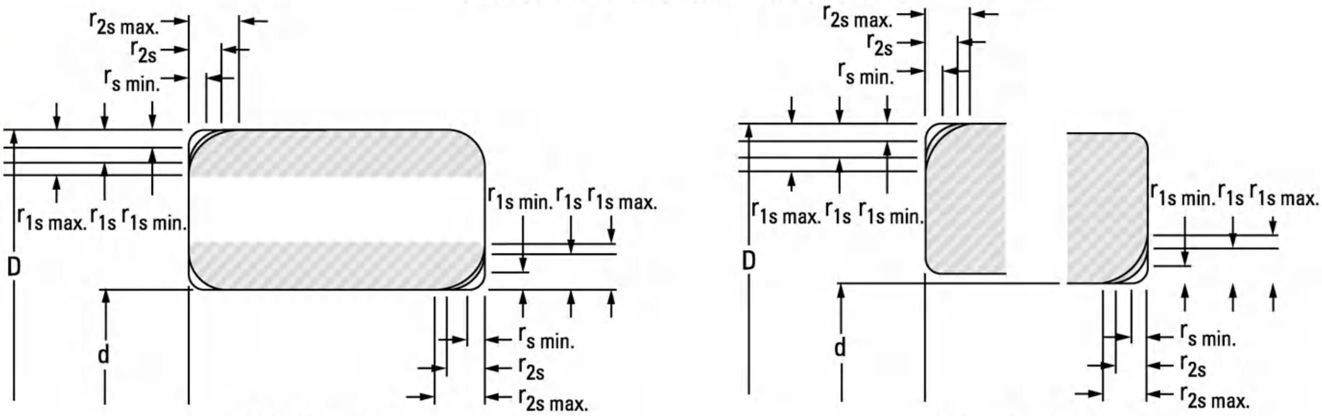
METRIC SERIES NEEDLE ROLLER BEARINGS (EXCEPT DRAWN CUP NEEDLE ROLLER BEARINGS)

Metric series needle roller bearings are available with Radial Internal Clearance (RIC) designations per either of the following tables: per "ISO/ABMA 'C' Clearance." Non-standard values also are available by special request. Standard radial internal clearance values are listed in the following tables based on bore size. The clearance required for a given application depends on the desired operating precision, rotational speed of the bearing and the fitting practice used. Most applications use a normal or C0 (Standard) clearance. Typically, larger clearance reduces the operating zone of the bearing, increases the maximum roller load and reduces the bearing's expected life.

Table A-7. Metric series needle roller bearing radial internal clearance limits

Bore		RIC							
		C2		C0 (Standard)		C3		C4	
over	incl.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
mm in	mm in	mm in	mm in	mm in	mm in	mm in	mm in	mm in	mm in
-	**30.000**	**0.025**	**0.000**	**0.045**	**0.020**	**0.060**	**0.035**	**0.075**	**0.050**
-	1.1811	0.0010	0.0000	0.0018	0.0008	0.0024	0.0014	0.0030	0.0020
30.000	**40.000**	**0.030**	**0.005**	**0.050**	**0.025**	**0.070**	**0.045**	**0.085**	**0.060**
1.1811	1.5748	0.0012	0.0002	0.0020	0.0010	0.0028	0.0018	0.0033	0.0024
40.000	**50.000**	**0.035**	**0.005**	**0.060**	**0.030**	**0.080**	**0.050**	**0.100**	**0.070**
1.5748	1.9685	0.0014	0.0002	0.0024	0.0012	0.0031	0.0020	0.0039	0.0028
50.000	**65.000**	**0.040**	**0.010**	**0.070**	**0.040**	**0.090**	**0.060**	**0.110**	**0.080**
1.9685	2.5591	0.0016	0.0004	0.0028	0.0016	0.0035	0.0024	0.0043	0.0031
65.000	**80.000**	**0.045**	**0.010**	**0.075**	**0.040**	**0.100**	**0.065**	**0.125**	**0.090**
2.5591	3.1496	0.0018	0.0004	0.0030	0.0016	0.0039	0.0026	0.0049	0.0035
80.000	**100.000**	**0.050**	**0.015**	**0.085**	**0.050**	**0.110**	**0.075**	**0.140**	**0.105**
3.1496	3.9370	0.0020	0.0006	0.0033	0.0020	0.0043	0.0030	0.0055	0.0041
100.000	**120.000**	**0.055**	**0.015**	**0.090**	**0.050**	**0.125**	**0.085**	**0.165**	**0.125**
3.9370	4.7244	0.0022	0.0006	0.0035	0.0020	0.0049	0.0033	0.0065	0.0049
120.000	**140.000**	**0.060**	**0.015**	**0.105**	**0.060**	**0.145**	**0.100**	**0.190**	**0.145**
4.7244	5.5118	0.0024	0.0006	0.0041	0.0024	0.0057	0.0039	0.0075	0.0057
140.000	**160.000**	**0.070**	**0.020**	**0.120**	**0.070**	**0.165**	**0.115**	**0.215**	**0.165**
5.5118	6.2992	0.0028	0.0008	0.0047	0.0028	0.0065	0.0045	0.0085	0.0065
160.000	**180.000**	**0.075**	**0.025**	**0.125**	**0.075**	**0.170**	**0.120**	**0.220**	**0.170**
6.2992	7.0866	0.0030	0.0010	0.0049	0.0030	0.0067	0.0047	0.0087	0.0067
180.000	**200.000**	**0.090**	**0.035**	**0.145**	**0.090**	**0.195**	**0.140**	**0.250**	**0.195**
7.0866	7.8740	0.0035	0.0014	0.0057	0.0035	0.0077	0.0055	0.0098	0.0077
200.000	**225.000**	**0.105**	**0.045**	**0.165**	**0.105**	**0.220**	**0.160**	**0.280**	**0.220**
7.8740	8.8583	0.0041	0.0018	0.0065	0.0041	0.0087	0.0063	0.0110	0.0087
225.000	**250.000**	**0.110**	**0.045**	**0.175**	**0.110**	**0.235**	**0.170**	**0.300**	**0.235**
8.8583	9.8425	0.0043	0.0018	0.0069	0.0043	0.0093	0.0067	0.0118	0.0093
250.000	**280.000**	**0.125**	**0.055**	**0.195**	**0.125**	**0.260**	**0.190**	**0.330**	**0.260**
9.8425	11.0236	0.0049	0.0022	0.0077	0.0049	0.0102	0.0075	0.0130	0.0102
280.000	**315.000**	**0.130**	**0.055**	**0.205**	**0.130**	**0.275**	**0.200**	**0.350**	**0.275**
11.0236	12.4016	0.0051	0.0022	0.0081	0.0051	0.0108	0.0079	0.0138	0.0108
315.000	**355.000**	**0.145**	**0.065**	**0.225**	**0.145**	**0.305**	**0.225**	**0.385**	**0.305**
12.4016	13.9764	0.0057	0.0026	0.0089	0.0057	0.0120	0.0089	0.0152	0.0120
355.000	**400.000**	**0.190**	**0.100**	**0.280**	**0.190**	**0.370**	**0.280**	**0.460**	**0.370**
13.9764	15.7480	0.0075	0.0039	0.0110	0.0075	0.0146	0.0110	0.0181	0.0146
400.000	**450.000**	**0.210**	**0.110**	**0.310**	**0.210**	**0.410**	**0.310**	**0.510**	**0.410**
15.7480	17.7165	0.0083	0.0043	0.0122	0.0083	0.0161	0.0122	0.0201	0.0161
450.000	**500.000**	**0.220**	**0.110**	**0.330**	**0.220**	**0.440**	**0.330**	**0.550**	**0.440**
17.7165	19.6850	0.0087	0.0043	0.0130	0.0087	0.0173	0.0130	0.0217	0.0173

METRIC SERIES BEARING CHAMFER DIMENSIONS



Radial Bearings

Thrust Bearings

Table A-8. Chamfer dimensions of radial bearings metric series

$r_{s\,min.}$	d Nominal bore dia. >	 ≤	$r_{1s\,max.}$	$r_{2s\,max.}$
mm in	mm in		mm in	mm in
0.150 0.0059	all all		0.300 0.0118	0.600 0.0236
0.200 0.0079	all all		0.500 0.0197	0.800 0.0315
0.300 0.0118	–	40.000 1.5748	0.600 0.0236	1.000 0.0394
	40.000 1.5748	–	0.800 0.0315	1.000 0.0394
0.600 0.0236	–	40.000 1.5748	1.000 0.0394	2.000 0.0787
	40.000 1.5748	–	1.300 0.0512	2.000 0.0787
1.000 0.0394	–	50.000 1.9685	1.500 0.0591	3.000 0.1181
	50.000 1.9685	–	1.900 0.0748	3.000 0.1181
1.100 0.0433	–	120.000 4.7244	2.000 0.0787	3.500 0.1378
	120.000 4.7244	–	2.500 0.0984	4.000 0.1575
1.500 0.0591	–	120.000 4.7244	2.300 0.09055	4.000 0.1575
	120.000 4.7244	–	3.000 0.1181	5.000 0.19685
2.000 0.0787	–	80.000 3.1496	3.000 0.1181	4.500 0.1772
	80.000 3.1496	220.000 8.6614	3.500 0.1378	5.000 0.19685
	220.000 8.6614	–	3.800 0.1496	6.000 0.2362
2.100 0.0827	–	280.000 11.0236	4.000 0.1575	6.500 0.2559
	280.000 11.0236	–	4.500 0.1772	7.000 0.2756

Table A-9. Chamfer dimensions of thrust bearings metric series

$r_{s\,min.}$	$r_{1s\,max.}$	$r_{2s\,max.}$
mm in	mm in	mm in
0.300 0.0118	0.800 0.0315	0.800 0.0315
0.600 0.0236	1.500 0.0591	1.500 0.0591
1.000 0.0394	2.200 0.0866	2.200 0.0866
1.100 0.0433	2.700 0.1063	2.700 0.1063
1.500 0.0591	3.500 0.1378	3.500 0.1378
2.000 0.0787	4.000 0.1575	4.000 0.1575

ABMA / ISO Symbols

- d — Bearing bore diameter, nominal and shaft-piloted washer bore diameter, nominal.
- D — Bearing outside diameter, nominal and housing-piloted washer outside diameter, nominal.
- $r_{s\,min.}$ — Smallest permissible single chamfer dimension (minimum limit).
- $r_{1s\,max.}$ — Largest permissible single chamfer dimension in a radial direction.
- $r_{2s\,max.}$ — Largest permissible single chamfer dimension in an axial direction.

A

SHAFT DESIGNS

BEARINGS WITHOUT INNER RINGS

When the shaft is used as the inner raceway for needle roller bearings it must have a hardness of 58 HRC or higher and a wave-free finish in order to realize the full load-carrying capability of the bearing.

1. **Metallurgy** – either case-hardening or through-hardening grades of good bearing-quality steel are satisfactory for raceways.

   To realize full bearing capacity, the raceway area must be at least surface hard with a reasonable core strength. During the carburizing or induction-hardening of case hardened steel, not only must the surface hardness requirement of 58 HRC or higher be met, but the basic concept is that the case depth with a hardness of HV 550 (52.3 HRC) must be 0.4 mm or higher. However, if the roller diameter is smaller than 4 mm, a case depth of (0.1 × Dw) mm or higher is recommended.
   (Dw:roller diameter)
2. **Strength** – the shaft must be of sufficient strength to keep the operating deflections within the limits outlined.
3. **Tolerance** – the suggested shaft diameter tolerances for each type of needle roller bearing are indicated in the appropriate section of this catalog.
4. **Variation of mean shaft diameter (taper)** – within the range of the bearing width, 5 μm or less per 25 mm or one-half the diameter tolerance or less (whichever is smaller).
5. **Deviation from circular form** – the radial deviation from true circular form of the raceway should not exceed 2.5 μm for diameters up to and including 25 mm. For raceways greater than 25 mm, the allowable radial deviation should not exceed 2.5 μm multiplied by a factor of the raceway diameter divided by 25.
6. **High frequency lobing** – the lobing that occurs 10 or more times around the circumference of a shaft and exceeds 0.4 μm from peak to valley is called chatter. Chatter usually causes undesirable noise and reduces fatigue life.
7. **Shaft slope** – Operating conditions which cause misalignment (shaft deflection, inaccuracy of shaft and housing, mounting errors) can affect bearing performance. For needle roller bearings, Table A-10 shows misalignment limitations based on bearing width.

Table A-10. Misalignment limitations

Bearing width		Maximum slope (mm/mm)	
mm	in.	Caged	Full complement
<25.4	<1	0.0015	0.0010
25.4 — 50.8	1 — 2	0.0010	0.0005
>50.8	>2	0.0005	0.0005

8. **Surface finish** – In addition to a wave-free finish, the raceway surface roughness of $R_a \leq 0.2$ μm must be maintained for the bearing to utilize its full load rating. The raceway area also must be free of nicks, burrs, scratches and dents. Oil holes are permissible in the raceway area, but care must be taken to blend the edges gently into the raceway, and if possible, the hole should be located in the unloaded zone of the raceway.

   Care also must be taken to prevent grind reliefs, fillets, etc., from extending into the raceway area. If the rollers overhang a grind relief or step on the shaft, there will be high stress concentration with resultant early damage.
9. **End chamfer** – for the most effective assembly of the shaft into a bearing, the end of the shaft should have a large chamfer or rounding. This should help in preventing damage to the roller complement, scratching of the raceway surface, and nicking of the shaft end.
10. **Sealing surface** – in some instances, bearings have integral or immediately adjacent seals that operate on the surface ground for the bearing raceway. Here, particular attention should be paid to the pattern of the shaft finish. In no instance should there be a "lead," or spiral effect, as often occurs with through-feed centerless grinding. Such a "lead" may pump lubricant past the seal.

BEARINGS WITH INNER RINGS

When it is undesirable or impractical to prepare the shaft to be used as a raceway, inner rings are available as listed in the tabular pages. If the shaft is not used directly as a raceway, the following design specifications must be met:

1. **Strength** – the shaft must be of sufficient strength to keep the operating deflections within the limits outlined.
2. **Tolerance** – the suggested shaft diameter tolerances for each type of needle roller bearing are indicated in the appropriate section of the catalog.
3. **Variation of mean shaft raceway diameter (taper) and deviation from circular form of the raceway** – should not exceed one-half the shaft diameter tolerance.
4. **Surface finish** – the surface finish should not exceed a roughness of Ra 0.8 μm.
5. **Locating shoulders or steps** – locating shoulders or steps in the shaft must be held to close concentricity with the bearing seat to prevent imbalance and resultant vibrations.

Table A-11. Shaft designs summary

	Shaft	
	Raceway surface	Fitting surface
Out-of-roundness	Shaft dia. ≤ 25 mm: 2.5 μm or less Shaft dia. > 25 mm: 2.5 μm × (shaft dia./25 mm) or less	One-half of shaft dia. tolerance or less
Variation of mean dia. (taper)	5 μm or less per 25 mm within the range of bearing width, or one-half of shaft dia. tolerance or less (whichever is smaller)	One-half of shaft dia. tolerance or less
Surface roughness	0.2a or less	0.8a or less
Hardness	58 HRC or harder[1)]	–

1) During the carburizing or induction-hardening of case hardened steel, not only must the surface hardness requirement of 58 HRC or higher be met, but the basic concept is that the case depth with a hardness of HV 550 (52.3 HRC) must be 0.4 mm or higher. However, if DW is smaller than 4 mm, a case depth of (0.1 × Dw) mm or higher is recommended. (Dw: roller dia.)

HOUSING DESIGNS

BEARINGS WITH OUTER RINGS

For bearings with outer rings, the function of the housing is to locate and support the outer ring. The following specifications must be met:

1. **Strength** – housings should be designed so that the radial loads placed on the bearings will cause a minimum of deflection or distortion of the housing.
2. **Variation of mean housing diameter (taper)** – within the width of the outer ring, 13 µm or one-half the diameter tolerance (whichever is smaller) or less.
3. **Deviation from circular form** – the housing bore should be round within one-half the housing bore tolerance.
4. **Parallelism** – when possible, line bore housings that are common to one shaft to obtain parallelism of the housing bores and the shaft axis.
5. **Surface finish** – The surface finish should not exceed R_a 1.6 µm.
6. **End chamfer** – to permit easy introduction of the bearing into the housing, the end of the housing should have a generous chamfer.

Only heavy-duty needle roller bearings can be installed into housings with a transition fit or a clearance fit. The outer ring should be a transition fit in the housing when it rotates relative to the load. The outer ring may be a clearance fit in the housing when it is stationary relative to the load. In either case, locate the bearings by shoulders, or other locating devices, to prevent axial movement.

Since only the heavy-duty needle roller bearing does not require an interference fit in the housing to round and size it properly, a split housing may be used if desired. Dowels should be used to maintain proper register of the housing sections.

Drawn cup needle roller bearings have a thin case-hardened outer ring that is out-of-round from the hardening operation. For proper mounting it must always be pressed into the housing. Split housings will not round and size a drawn cup bearing. When split housings must be used, the bearing should first be mounted in a cylindrical sleeve.

The housing should be of sufficient tensile strength and section to round and size the bearing. It must be designed for minimum distortion under load. Steel or cast iron housings are preferred.

Housing bores in low tensile strength materials such as aluminum, magnesium, phenolics, etc., should be reduced to provide more interference fit. Thin section cast iron and steel housings may also require reduced bores. Consult your representative for suggestions when working with these lower strength housings.

The housing should be through-bored if possible. When shouldered housing bores are unavoidable, the bearing should be located far enough from the shoulder to avoid the danger of crushing the end of the drawn cup during installation.

When the drawn cup bearing is mounted close to the housing face, care should be taken to mount the bearing at least 0.250 mm (0.0100 in) within the housing face to protect the bearing lip.

BEARINGS WITHOUT OUTER RINGS

In many cases, such as with gear bores, it is desirable to have the housing bore serve as the outer raceway for radial needle roller and cage assemblies or loose needle roller complements. In those instances, as for shafts used as raceways, the housing bore must have a hardness of 58 HRC or harder and a surface roughness Ra ≤ 0.2 µm so that the full load-carrying capacity of the bearing is realized.

1. **Strength** – the housing must be of sufficient cross section to maintain proper roundness and running clearance under maximum load.
2. **Metallurgical** – material selection, hardness and case depth should be consistent with the requirements for inner raceways given in the shaft design.
3. **Variation of mean housing raceway diameter (taper)** – within the range of the bearing width, 5 µm or less per 25 mm or one-half the housing bore diameter tolerance or less (whichever is smaller). In addition, the bore diameter must never be smaller at both ends than in the center [sway-back].
4. **Deviation from circular form** – the raceway out-of-roundness should not exceed one-half the bore tolerance.
5. **Surface finish** – In addition to a wave-free finish, the raceway surface roughness of Ra ≤ 0.2 µm must be maintained for the bearing to utilize its full load rating. The raceway area also must be free of nicks, burrs, scratches and dents.
6. **Grind reliefs** – care must be exercised to ensure that grind reliefs, fillets, etc., do not extend to the raceway. Oil holes in the raceway area are permissible, but the edges must be blended smoothly with the raceway and, if possible, the hole should be located in the unloaded zone of the raceway.

Table A-12. Housing designs summary

	Housing bore	
	Raceway surface	Fitting surface
Out-of-roundness	One-half of bore tolerance or less	One-half of bore tolerance or less
Variation of mean dia. (taper)	5 µm or less per 25 mm within the range of outer ring width, or one-half of bore tolerance or less (whichever is smaller)	13 µm or less within the range of outer ring width, or one-half of bore tolerance or less (whichever is smaller)
Surface roughness	0.2a or less	1.6a or less
Hardness	58 HRC or harder[1)]	–

1) During the carburizing or induction-hardening of case hardened steel, not only must the surface hardness requirement of 58 HRC or higher be met, but the basic concept is that the case depth with a hardness of HV 550 (52.3 HRC) must be 0.4 mm or higher. However, if DW is smaller than 4 mm, a case depth of (0.1 × Dw) mm or higher is recommended. (Dw: roller dia.)

FITS

The purpose of fit is to securely fix the inner or outer ring to the shaft or housing, to preclude detrimental circumferential sliding on the fitting surface.

Such detrimental sliding (referred to as "creep") will cause abnormal heat generation, wear of the fitting surface, infiltration of abrasion metal particles into the bearing, vibration, and many other harmful effects, which cause a deterioration of bearing functions.

FIT SELECTION

In selecting the proper fit, careful consideration should be given to bearing operating conditions.
Major specific considerations are :

- Direction of load
- Load characteristics and magnitude
- Temperature distribution in operating
- Bearing internal clearance
- Surface finish, material and thickness of shaft and housing
- Mounting and dismounting methods
- Necessity to compensate for shaft thermal expansion at the fitting surface
- Bearing type and size

In view of these considerations, the following paragraphs explain the details of the important factors in fit selection.

1. Direction of load

Direction of load classified into three types : rotating inner ring load; rotating outer ring load and indeterminate direction load.
Table A-13 tabulates the relationship between these characteristics and fit.

Table A-13. Direction of Load and Fits

Direction of load		Rotating Ring		Type of load	Fit	
		Inner ring	outer ring		Inner ring	outer ring
Rotating inner ring load	Inner ring : Circumferential load Outer ring : Point load	Rotating	Stationary	Rotating load	Tight	Loose
Rotating outer ring load	Inner ring : Point load Outer ring : Circumferential load	Stationary	Rotating	Rotating load	Loose	Tight
Indetermi-nate direction load	Inner ring : Circumferential load Outer ring : Oscillating load	Rotating Stationary	Stationary Rotating	Stationary load > Rotating load Stationary load < Rotating load	Tight	Slightly tight
	Inner ring : Oscillating load Outer ring : Circumferential load	Rotating Stationary	Stationary Rotating	Stationary load > Rotating load Stationary load < Rotating load	Slightly tight	Tight

2. Effect of load characteristic and magnitude

When a radial load is applied, the inner ring will expand slightly. Since this expansion enlarges the circumference of the bore minutely, the initial interference is reduced.

The reduction can be calculated by the following equations :

[in the case of $F_r \leqq 0.25\ C_0$]

$$\Delta_{dF} = 0.08\sqrt{\frac{d}{B}} \cdot F_r \times 10^{-3}$$

[in the case of $F_r > 0.25\ C_0$]

$$\Delta_{dF} = 0.02\frac{F_r}{B} \times 10^{-3}$$

where :

Δ_{dF}	: Reduction of inner ring interference	mm
d	: Nominal bore diameter of bearing	mm
B	: Nominal inner ring width	mm
F_r	: Radial load	N
C_0	: Basic static load rating	N

When the radial load exceeds the C_0 value by 25%, greater interference is needed. When impact loads are expected, much greater interference is needed.

3. Effect of fitting surface roughness

The effective interference obtained after fitting differs from calculated interference due to plastic deformation of the ring fitting surface. When the inner ring is fitted, the effective interference, subject to the effect of the fitting surface finish, can be approximated by the following equations :

[In the case of a ground shaft]

$$\Delta_{deff} \doteqdot \frac{d}{d+2}\Delta_d$$

[In the case of a turned shaft]

$$\Delta_{deff} \doteqdot \frac{d}{d+3}\Delta_d$$

where :

Δ_{deff}	: Effective interference	mm
Δ_d	: Calculated interference	mm
d	: Nominal bore diameter of bearing	mm

A

4. Effect of temperature

A bearing generally has an operating temperature that is higher than the ambient temperature. When the inner ring operates under load, its temperature generally becomes higher than that of the shaft and the effective interference decreases due to the greater thermal expansion of the inner ring.

If the temperature difference between the bearing inside and surrounding housing is $\varDelta t$, the temperature difference between the fitting surfaces of the inner ring and shaft will be approximately (0.10 to 0.15) × $\varDelta t$. The reduction of interference ($\varDelta dt$) due to the temperature difference is then expressed as follows:

$$\varDelta_{dt} = (0.10 \sim 0.15)\ \varDelta_t \cdot \alpha \cdot d$$
$$\fallingdotseq 0.001\,5\ \varDelta_t \cdot d \times 10^{-3}$$

In this equation,

- $\varDelta_{dt}$: Reduction of interference due to temperature difference mm
- $\varDelta_t$: Temperature difference between the inside of the bearing and the surrounding housing °C
- α : Linear expansion coefficient of bearing steel (approximately equal to 12.5×10^{-6}) 1/°C
- d : Nominal bore diameter of bearing mm

Consequently, when a bearing is higher in temperature than the shaft, greater interference is required.

However, a difference in temperature or in the coefficient of expansion may sometimes increase the interference between the outer ring and housing. Therefore, care should be taken when clearance is provided to accommodate shaft thermal expansion.

5. Maximum stress due to fit

When a bearing is fitted with interference, the bearing ring will expand or contract, generating internal stress.

Should this stress be excessive, the bearing ring may fracture.

The maximum bearing fitting-generated stress is determined by the equation in Table A-14.

In general, to avoid fracture, it is best to adjust the maximum interference to less than 1/1 000 of the shaft diameter, or the maximum stress (σ), determined by the equation in Table A-14, should be less than 120 MPa.

Table A-14 does not apply to drawn cup needle roller bearings.

Recommended Fits

Recommended fits are listed in each bearing section and within the tabular pages.

Table A-14. Maximum fitting-generated stress in bearings

Shaft & inner ring	Housing bore & outer ring
(In the case of hollow shaft) $\sigma = \frac{E}{2} \cdot \frac{\varDelta_{deff}}{d} \cdot \frac{\left(1 - \frac{d_0^2}{d^2}\right)\left(1 + \frac{d^2}{D_i^2}\right)}{\left(1 - \frac{d_0^2}{D_i^2}\right)}$	**(In the case of $D_h \neq \infty$)** $\sigma = E \cdot \frac{\varDelta_{Deff}}{D} \cdot \frac{\left(1 - \frac{D^2}{D_h^2}\right)}{\left(1 - \frac{D_e^2}{D_h^2}\right)}$
(In the case of solid shaft) $\sigma = \frac{E}{2} \cdot \frac{\varDelta_{deff}}{d} \cdot \left(1 + \frac{d^2}{D_i^2}\right)$	**(In the case of $D_h = \infty$)** $\sigma = E \cdot \frac{\varDelta_{Deff}}{D}$

where :

- σ : Maximum stress MPa
- d : Nominal bore diameter (shaft diameter) mm
- D_i : Raceway contact diameter of inner ring mm
  roller bearing … $D_i \fallingdotseq 0.25\,(D + 3d)$
- $\varDelta_{deff}$: Effective interference of inner ring mm
- d_0 : Bore diameter of hollow shaft mm
- D_e : Raceway contact diameter of outer ring mm
  roller bearing … $De \fallingdotseq 0.25\,(3D + d)$
- D : Nominal outside diameter (bore diameter of housing) mm
- $\varDelta_{Deff}$: Effective interference of outer ring mm
- D_h : Outside diameter of housing mm
- E : Young's modulus = 2.08×10^5 MPa

[Remark] The above equations are applicable when the shaft and housing are steel.
When other materials are used, JTEKT should be consulted.

CLEARANCE

Bearing internal clearance is defined as the clearance between the bearing ring and the rolling elements. The total distance either inner or outer ring can be moved when the specified measuring load is applied to the ring in radial direction and the other ring is fixed is defined as radial internal clearance.

The term "residual clearance" is also defined as the original clearance decreased owing to expansion or contraction of a raceway due to fitting, when the bearing is mounted in the shaft and housing.

The term "effective clearance" is defined as the residual clearance decreased owing to dimensional change arising from temperature differentials within the bearing.

The term "operating clearance" is defined as the internal clearance present while a bearing mounted in a machine is rotating under a certain load, or, the effective clearance increased due to elastic deformation arising from bearing loads.

The operating clearance is closely related to bearing performance and life. It is therefore desirable to select a clearance with a lower limit value on the positive side of zero.

When selecting the clearance, fitting conditions, temperature conditions, and tolerance of mounting dimensions must all be taken into account.

The operating clearance can be obtained from the equation in Table A-15.

These calculations can be used for machined ring needle roller bearings but not for drawn cup needle roller bearings.

For the drawn cup needle roller bearings refer to page B-2-7.

Table A-15. Operating clearance

Operating clearance (S)	$S = S_o - (S_f + S_{t1} + S_{t2}) + S_w$*	* [S_w (increase of clearance due to load) is generally small, and thus may be ignored, although there is a equation for determining the value.]
Decrease of clearance due to fitting (S_f)	**(In the case of hollow shaft)** $S_{fi} = \varDelta_{deff} \frac{d}{D_i} \cdot \frac{\left(1 - \frac{{d_0}^2}{d^2}\right)}{\left(1 - \frac{{d_0}^2}{{D_i}^2}\right)}$ **(In the case of solid shaft)** $S_{fi} = \varDelta_{deff} \frac{d}{D_i}$	**(In the case of $D_h \neq \infty$)** $S_{fo} = \varDelta_{Deff} \frac{D_e}{D} \cdot \frac{\left(1 - \frac{D^2}{{D_h}^2}\right)}{\left(1 - \frac{{D_e}^2}{{D_h}^2}\right)}$ **(In the case of $D_h = \infty$)** $S_{fo} = \varDelta_{Deff} \frac{D_e}{D}$
Decrease of clearance due to temperature differentials between inner and outer rings (S_{t1})	The amount of decrease varies depending on the state of housing; however, generally the amount can be approximated by the following equation on the assumption that the outer ring will not expand : $S_{t1} = \alpha (D_i \cdot t_i - D_e \cdot t_e)$	where : $D_e = D_i + 2D_w$ Consequently, $S_{t1} + S_{t2}$ will be determined by the following equation : $S_{t1} + S_{t2} = \alpha \cdot D_i \cdot t_1 + 2\alpha \cdot D_w \cdot t_2$ (Temperature differential between the inner and outer rings, t1, can be expressed as follows : $t_1 = t_i - t_e$ Temperature differential between the rolling element and outer ring, t2, can be expressed as follows : $t_2 = t_w - t_e$)
Decrease of clearance due to temperature rise of rolling element (S_{t2})	$S_{t2} = 2\alpha \cdot D_w \cdot t_w$	

In Table A-15,

- S : Operating clearance — mm
- S_o : Clearance before mounting — mm
- S_f : Decrease of clearance due to fitting — mm
- S_{fi} : Expansion of inner ring raceway contact diameter — mm
- S_{fo} : Contraction of outer ring raceway contact diameter — mm
- S_{t1} : Decrease of clearance due to temperature differentials between inner and outer rings — mm
- S_{t2} : Decrease of clearance due to temperature rise of the rolling elements — mm
- S_w : Increase of clearance due to load — mm
- $\varDelta_{deff}$: Effective interference of inner ring — mm
- d : Nominal bore diameter (shaft diameter) — mm
- d_0 : Bore diameter of hollow shaft — mm
- D_i : Inner ring raceway contact diameter — mm
  roller bearing … $D_i \fallingdotseq 0.25\,(D + 3d)$
- $\varDelta_{Deff}$: Effective interference of outer ring — mm
- D_h : Outside diameter of housing — mm
- D_e : Outer ring raceway contact diameter — mm
  roller bearing … $D_e \fallingdotseq 0.25\,(3D + d)$
- D : Nominal outside diameter — mm
- α : Linear expansion coeffi cient of bearing steel (12.5×10^{-6}) — 1/°C
- D_w : Average diameter of rolling elements — mm
  roller bearing … $D_w \fallingdotseq 0.25\,(D - d)$
- t_i : Temperature rise of the inner ring — °C
- t_e : Temperature rise of the outer ring — °C
- t_w : Temperature rise of rolling elements — °C

■ Bearings are sometimes used with a non-steel shaft or housing.
In the automotive industry, a statistical method is often incorporated for selection of clearance.
In these cases, or when other special operating conditions are involved, JTEKT should be consulted.

LUBRICATION

PURPOSE OF LUBRICATION

Lubrication is one of the most important factors determining bearing performance. Since the suitability of the lubricant and lubrication method have a dominant influence on bearing life, the most suitable lubricant should be selected according to operating conditions.

Functions of lubrication :

- To lubricate each part of the bearing, and to reduce friction and wear
- To carry away heat generated inside bearing due to friction and other causes
- To cover rolling contact surface with the proper oil film in order to prolong bearing fatigue life
- To prevent corrosion and contamination by dirt

Although the same general rules for ball bearings and roller bearings can also be applied to needle roller bearing lubrication, the following points should also be considered :

- The space in the bearing is very small; thus, only a little lubricant can be retained.
- The bearing is relatively wide, so circulating the lubricant through the bearing is difficult.
- In the case of full complement type sliding contact between rollers may arise.
- Rollers may skew during rotation.
- Often used in the application where oscillating motion is present.

Accordingly, these points must be given sufficient consideration when selecting the lubricant and method of lubrication.

LUBRICANT

Bearing lubrication is classified broadly into two categories : grease lubrication and oil lubrication. Table A-16 makes a general comparison between the two.

Table A-16. Comparison between grease and oil lubrication

Item	Grease	Oil
Sealing device	Easy	Slightly complicated and special care required for maintenance
Lubricating ability	Good	Excellent
Rotation speed	Low/medium speed	Applicable at high speed as well
Replacement of lubricant	Slightly troublesome	Easy
Life of lubricant	Relatively short	Long
Cooling effect	No cooling effect	Good (circulation is necessary)
Filtration of dirt	Difficult	Easy

GREASE LUBRICATION

Grease is made by mixing and dispersing a solid of high oil-affinity (called a thickener) with lubricant oil (as a base), and transforming it into a semi-solid state.

As well, a variety of additives can be added to improve specific performance.

Many types of grease are marketed in various combinations of thickener, base oil and additives according to the purposes. So, it is very important to select proper types of grease.

The characteristics of various greases are shown in Table A-17.

Table A-17. Characteristics of respective greases

	Lithium grease			Calcium grease (cup grease)	Sodium grease (fiber grease)	Complex base grease		Non-soap base grease		
Thickener	Lithium soap			Calcium soap	Sodium soap	Lithium complex soap	Calcium complex soap	Bentone	Urea compounds	Fluorine compounds
Base oil	Mineral oil	Synthetic oil (diester oil)	Synthetic oil (silicon oil)	Mineral oil	Mineral oil	Mineral oil	Mineral oil	Mineral oil	Mineral/ synthetic oil	Synthetic oil
Dropping point (°C)	170 to 190	170 to 230	220 to 260	80 to 100	160 to 180	250 or higher	200 to 280	–	240 or higher	250 or higher
Operating temperature range (°C)	–30 to +120	–50 to +130	–50 to +180	–10 to +70	0 to +110	–30 to +150	–10 to +130	–10 to +150	–30 to +150	–40 to +250
Rotation speed range	Medium to high	High	Low to medium	Low to medium	Low to high	Low to high	Low to medium	Medium to high	Low to high	Low to medium
Mechanical stability	Excellent	Good to excellent	Good	Fair to good	Good to excellent	Good to excellent	Good	Good	Good to excellent	Good
Water resistance	Good	Good	Good	Good	Bad	Good to excellent	Good	Good	Good to excellent	Good
Pressure resistance	Good	Fair	Bad to fair	Fair	Good to excellent	Good	Good	Good to excellent	Good to excellent	Good
Remarks	Most widely usable for various rolling bearings.	Superior low temperature and friction characteristics.	Superior high and low temperature characteristics.	Suitable for applications at low rotation speed and under light load. Not applicable at high temperature.	Liable to emulsify in the presence of water. Used at relatively high temperature.	Superior mechanical stability and heat resistance. Used at relatively high temperature.	Superior pressure resistance when extreme pressure agent is added.	Suitable for applications at high temperature and under relatively heavy load.	Superior water resistance, oxidation stability, and heat stability. Suitable for applications at high temperature and high speed.	Superior chemical resistance and solvent resistance. Usable at up to 250 °C.

(1) Base oil

Mineral oil is usually used as the base oil for grease.

When low temperature fluidity, high temperature stability, or other special performance is required, diester oil, silicon oil, polyglycolic oil, fluorinated oil, or other synthetic oil is often used.

Generally, grease with a low viscosity base oil is suitable for applications at low temperature or high rotation speed; grease with high viscosity base oils are suitable for applications at high temperature or under heavy load.

(2) Thickener

Most greases use a metallic soap base such as lithium, sodium, or calcium as thickeners. For some applications, however, non-soap base thickeners (inorganic substances such as bentone, silica gel, and organic substances such as urea compounds, fluorine compounds) are also used.

In general, the mechanical stability, bearing operating temperature range, water resistance, and other characteristics of grease are determined by the thickener.

(Lithium soap base grease)
Superior in heat resistance, water resistance and mechanical stability.

(Calcium soap base grease)
Superior in water resistance; inferior in heat resistance.

(Sodium soap base grease)
Superior in heat resistance; inferior in water resistance.

(Non-soap base grease)
Superior in heat resistance.

(3) Additives

Various additives are selectively used to serve the respective purposes of grease applications.

- Extreme pressure agents
  When bearings must tolerate heavy or impact loads.
- Oxidation inhibitors
  When grease is not refilled for a long period.

Structure stabilizers, rust preventives, and corrosion inhibitors are also used.

(4) Consistency

Consistency, which indicates grease hardness, is expressed as a figure obtained, in accordance with ASTM (JIS), by multiplication by 10 the depth (in mm) to which the cone-shaped metallic plunger penetrates into the grease at 25 °C by deadweight in 5 seconds. The softer the grease, the higher the figure.

Table A-18 shows the relationships between the NLGI scales and ASTM (JIS) penetration indexes, service conditions of grease.

(NLGI : National Lubricating Grease Institute)

It is imperative that the bearing operating temperature is always within the temperature range specified for the grease used. Although softer greases provide better lubrication, they are more likely to be churned. Since grease churning tends to cause temperature rise and leakage, this characteristic should be taken into account when selecting grease consistency. For ordinary operating conditions, greases of NLGI No. 0 to 3 are commonly used. When the bearing operating speed is higher, a somewhat harder grease with high mechanical stability should be selected.

Table A-18. Grease consistency and service conditions

ASTM (JIS) penetration index (25 °C, 60 mixing operations)	NLGI scale	Service conditions/applications
355 - 385	0	For centralized lubricating
310 - 340	1	For centralized lubricating, at low temperature
265 - 295	2	For general use
220 - 250	3	For general use, at high temperature
175 - 205	4	For special applications

[Note] The larger the penetration index, the softer is the grease.

(5) Mixing of different greases

Since mixing of different greases changes their properties, greases of different brands should not be mixed.

If mixing cannot be avoided, greases containing the same thickener should be used. Even if the mixed greases contain the same thickener, however, mixing may still produce adverse effects, due to difference in additives or other factors.

Thus it is necessary to check the effects of a mixture in advance, through testing or other methods.

A

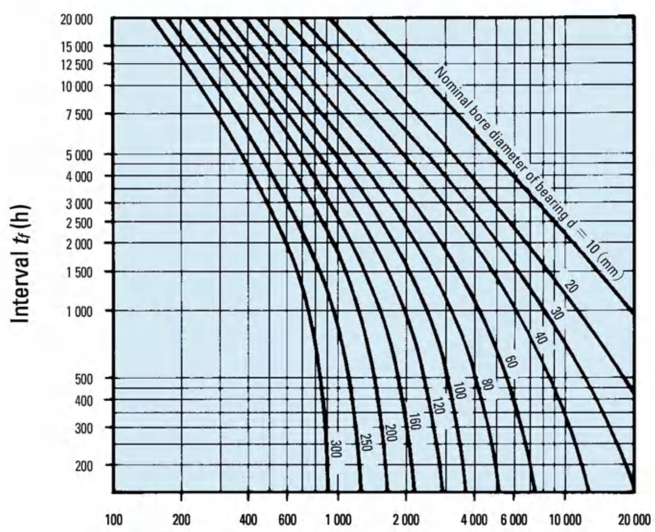
REPLENISHMENT/REPLACEMENT OF GREASE

The method of replenishing/replacing grease depends largely on the lubrication method. Whichever method may be utilized, care should be taken to use clean grease and to keep dirt or other foreign matter out of the housing.

When grease is refilled, new grease must be injected inside bearing.

In case of high speed operation or a small air space, because it is necessary to replenish grease often, a grease inlet should be provided as near the bearing as possible so that the deteriorated grease may be replaced by new grease.

Under normal operating conditions, grease life may be approximated by the graphs shown in Fig. A-13. It is recommended you use this diagram as a guide for replenishment and replacement of grease.

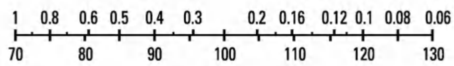


■ Temperature correction

When the bearing operating temperature exceeds 70 °C, t_f', obtained by multiplying t_f by correction coefficient a, found on the scale below, should be applied as the feeding interval.

$$t_f' = t_f \cdot a$$

Temperature correction coefficient a



Bearing operating temperature T °C

Fig. A-13 Grease feeding interval

⚠ WARNING
Mixing grease types can cause the lubricant to become ineffective, hich can result in equipment failure, creating a risk of serious bodily harm.

LUBRICATING OIL

The most commonly used bearing lubricating oil is super refined mineral oil, which has excellent oxidation stability and rust inhibition as well as high film strength. However, as bearings are being used in a variety of applications, a wide variety of synthetic oils are being used. What's more, a variety of additives (such as oxidation inhibitors, rust inhibitors, and anti-foam agents) are being used to improve the specific properties of these synthetic oils. Table A-19 shows the properties of various lubricating oils.

Table A-19. Properties of various lubricating oils

Lubricating oil type	Super refined mineral oil	Major synthetic oils				
		Diester oil	Silicon oil	Polyglycolic oil	Polyphenyl ether oil	Fluorinated oil
Bearing operating temperature range (˚C)	**–40 to +220**	**–55 to +150**	**–70 to +350**	**–30 to +150**	**0 to +330**	**–20 to +300**
Lubricating ability	Excellent	Excellent	Fair	Good	Good	Excellent
Oxidation stability	Good	Good	Fair	Fair	Excellent	Excellent
Radiation resistance	Bad	Bad	Bad to fair	Bad	Excellent	–

LUBRICATING OIL SELECTION

The most important thing to consider when selecting a lubricating oil is to select an oil that has a viscosity that is appropriate for the operating temperature of the bearing.

Use Table A-20 to select the proper kinematic viscosity for your bearing operating conditions. Use this value as a guideline.

If the viscosity of the lubricating oil is too low, an insufficient oil film will form. If the viscosity of the lubricating oil is too high, heat will be generated due to viscous resistance.

Generally, the larger the load or the higher the operating temperature, the higher the viscosity of the used lubricating oil and the higher the rotational speed, the lower the viscosity of the used lubricating oil.

The relationship between the lubricating oil viscosity and temperature is shown in Fig. A-14.

Table A-20. Proper kinematic viscosities by bearing operating conditions

Operating temperature	$d_m n$ value	Proper kinematic viscosity (expressed in the ISO viscosity grade or the SAE No.)			
		Light/normal load		Heavy/impact load	
–30 to 0°C	All rotation speeds	ISO VG 15, 22, 46	(Refrigerating Machine oil)	——	
0 to 60°C	300 000 or lower	ISO VG 46	(Bearing oil Turbine oil)	ISO VG 68 SAE 30	(Bearing oil Turbine oil)
	300 000 to 600 000	ISO VG 32	(Bearing oil Turbine oil)	ISO VG 68	(Bearing oil Turbine oil)
	600 000 or higher	ISO VG 7, 10, 22	(Bearing oil)	——	
60 to 100°C	300 000 or lower	ISO VG 68	(Bearing oil)	ISO VG 68, 100 SAE 30	(Bearing oil)
	300 000 to 600 000	ISO VG 32, 46	(Bearing oil Turbine oil)	ISO VG 68	(Bearing oil Turbine oil)
	600 000 or higher	ISO VG 22, 32, 46	(Bearing oil Turbine oil Machine oil)	——	
100 to 150°C	300 000 or lower	ISO VG 68, 100 SAE 30, 40	(Bearing oil)	ISO VG 100 to 460	(Bearing oil Gear oil)
	300 000 to 600 000	ISO VG 68 SAE 30	(Bearing oil Turbine oil)	ISO VG 68, 100 SAE 30, 40	(Bearing oil)

[Remarks] 1. $d_m n = \frac{D+d}{2} \times n$......... {$D$: nominal outside diameter (mm), d : nominal bore diameter (mm), n : rotational speed (min^{-1})}
2. Please contact with JTEKT if the bearing operating temperature is under –30 °C or over 150 °C.

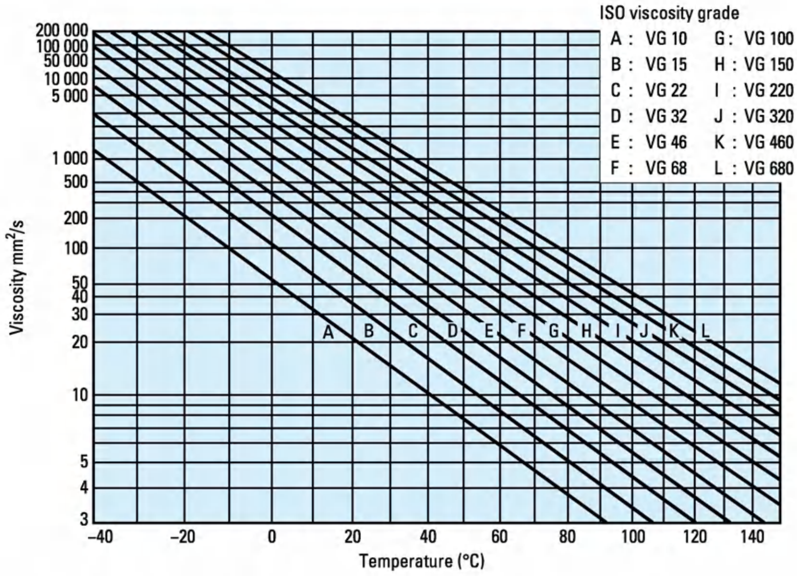


Fig. A-14. Relationship between lubricating oil viscosity and temperature (viscosity index : 100)

CLASSIFICATION

There are several classifications of oils based on viscosity grades. The most familiar are the Society of Automotive Engineers (SAE) classifications for automotive engine and gear oils. The American Society for Testing and Materials (ASTM) and the International Organization for Standardization (ISO) have adopted standard viscosity grades for industrial fluids. Fig. A-15 shows the viscosity comparisons of ISO/ASTM with SAE classification systems at 40°C (104˚F).

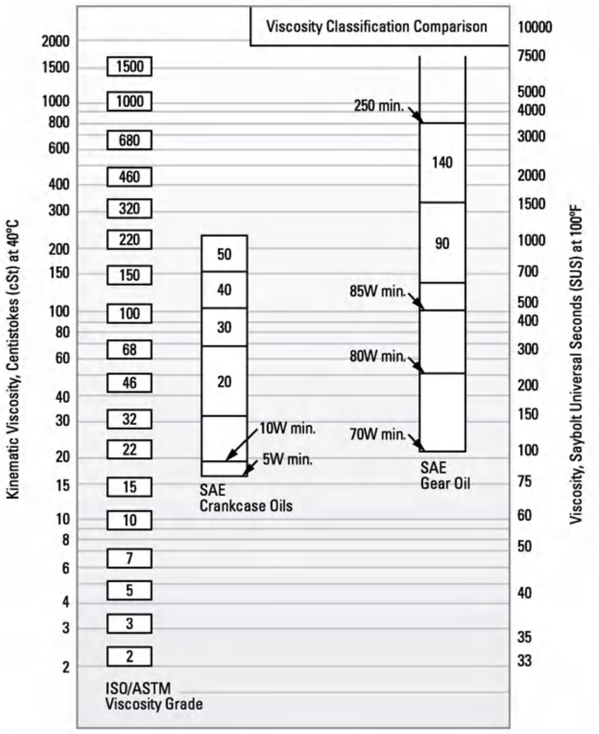


Fig. A-15. Viscosity classification comparison between ISO/ASTM grades (ISO 3448/ASTM D2442) and SAE grades (SAE J 300-80 for crankcase oils, SAE J 306-81 for axle and manual transmission oils)

OIL LUBRICATION METHOD

Oil lubrication is usable even with high speed rotation and at somewhat high temperatures and is effective in reducing bearing vibration and noise. Therefore, oil lubrication is used in many cases where grease lubrication does not work.

The main types and methods of oil lubrication are shown in Table A-21.

Table A-21. Types and methods of oil lubrication

Oil bath	• This is the simplest method. Bearings are soaked in oil before operation. • This method is applicable for low and medium rotational speeds. • Attaching an oil level gauge makes it possible to adjust the oil amount. • For horizontal shafts, approximately half of the rolling element in the lowest position is immersed. For vertical shafts, approximately 70 to 80% of the bearings are immersed. • Using magnetic lids is advantageous as it prevents iron powder generated by friction from being dispersed in the oil.
Oil drip	• An oiler is used to drip the oil, and the rotating parts are operated to fill the inside of the housing with an oil mist, which also has a cooling effect. • This method can be used with up to relatively high speeds and medium-sized loads. • The most common example of this method uses five to six drops of oil per minute. (It is difficult to adjust the amount of oil used to 1 mL/h or less.) • Ensure that oil does not accumulate in the bottom of the housing.
Oil splash	• A simple flinger or gears are attached to the shaft to supply the oil to its destination by means of flinging or splashing operations. This method can be used to supply oil even to bearings that are far away from the oil tank. • This method can be used with up to relatively high speeds. • The oil level must be maintained within a certain range. • Using magnetic lids is advantageous as it prevents iron powder generated by friction from being dispersed in the oil. What's more, to prevent the intrusion of foreign materials into the bearing, it is advisable to use a shield board or baffle.
Forced oil circulation	• This method uses an oil circulation system. After the supplied oil lubricates and cools the inside of the bearing, the oil passes through the oil return pipe to the tank. The oil is filtered and cooled and is then forcibly supplied once more by way of a pump. • This method is used a great deal under high rotational speed and high temperature conditions. • To prevent the lubricating oil from accumulating inside the housing, it is advisable to make the oil return pipe approximately twice as thick as the oil supply pipe.
Oil jet	• In this method, oil is sprayed from nozzles at a constant pressure (approximately 0.1 to 0.5 MPa). This method provides a large cooling effect. • This method is applicable for high rotational speeds and heavy loads. • Generally, the nozzle diameters are between 0.5 and 2 mm, and nozzles are installed in positions between 5 and 10 mm from the sides of the bearings. It is advisable to use between 2 and 4 nozzles for situations in which a large amount of heat is generated. • The oil jet method supplies a large quantity of oil, so it is advisable to use an oil discharge pump to forcibly discharge oil in order to prevent against the stagnation of unnecessary oil.
Oil mist lubrication (fog lubrication)	• In this method, dry mist (air that contains oil in mist form) obtained from an oil mist generator is continuously sent to the location where oil is to be applied to the bearing. The dry mist is then changed to wet mist (oil drops that can easily be affixed to a surface) by the nozzles attached to the housing or bearing, and the oil is then applied to the bearing. • This method forms and retains the minimum necessary oil film for lubrication, which provides benefits such as prevention of oil pollution, simplification of bearing maintenance, extension of bearing fatigue life, and reduction of oil consumption.
Oil and air lubrication	• In this method, a metering piston is used to eject a minuscule amount of oil, a mixing valve is used to mix the oil with compressed air, and the oil and air mixture is then applied to the bearing continuously and stably. • It's possible to perform metering management of the minuscule amount of oil, so new lubricating oil can always be supplied. Therefore, this method is applicable to usages with high rotational speeds such as machine tool main spindles. • The spindle's internal pressure rises because compressed air is supplied together with the lubricating oil. Therefore, this method is also effective at preventing the intrusion of external materials such as debris and cutting fluid. What's more, the lubricating oil flows through the oil supply pipe, so this method results in an extremely small amount of air pollution.

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LIMITING SPEEDS

In addition to the bearing load ratings, the tabular pages also list the limiting speed values which are the maximum speeds at which the bearings may operate. These speeds have been calculated for unsealed and sealed bearings of conventional design, tolerances and internal clearances, properly mounted with low applied loads using normal splash, drip feed or other methods of lubrication which will provide adequate cooling of the bearings. A bearing may operate at a speed higher than the listed limiting speed with the use of a clean, good quality oil and after prior consultation with JTEKT's Engineering Department. With high speeds and high acceleration rates, the ratio of P/C should not fall below 0.02 to prevent skidding of the rolling elements.

Also the bearing should not be subjected to uneven stress distribution due to the effects of misalignment between the bearing housings, deformation of the shaft or housing.

Speeds Inadequate for Elastohydrodynamic Lubricating Film

International Standard ISO 281 which covers calculation of dynamic load ratings and rating life states that at exceptionally low rotational speeds (i.e. the product of speed and pitch diameter (D_{pw}) in mm is less than 10000) the generated lubricant film is unlikely to be adequate to separate the rolling element/raceway contacts. At such operating conditions it may be inappropriate to calculate the bearing life although practical improvement in life, may be achieved with the use of lubricants of higher kinematic viscosity or containing EP additives.

BEARING TOLERANCES, INCH AND METRIC

TOLERANCES OF NEEDLE ROLLER BEARINGS

The tolerances given in the following table apply to the rings of needle roller radial bearing types whose rings are precision finished.

TOLERANCE TERMS, SYMBOLS AND DEFINITIONS
Axes, planes etc.

Inner ring axis: Axis of the cylinder inscribed in a basically cylindrical bore. The inner ring axis is also the bearing axis.

Outer ring axis: Axis of the cylinder circumscribed around a basically cylindrical outside surface.

Radial plane: Plane perpendicular to the bearing or ring axis. It is, however, acceptable to consider radial planes referred to in the definitions as being parallel with the plane tangential to the reference face of a ring or the back face of a thrust bearing washer.

Radial direction: Direction through the bearing or ring axis in a radial plane.

Axial plane: Plane containing the bearing or ring axis.

Axial direction: Direction parallel with the bearing or ring axis. It is, however, acceptable to consider axial directions referred to in the definitions as being perpendicular to the plane tangential to the reference face of a ring or the back face of a thrust bearing washer.

Reference face: Face designated by the manufacturer of the bearings and that may be used as the reference face in measurements.

The reference face for measurement is generally taken as the unmarked face. In case of symmetrical rings, when it is not possible to identify the reference face, the tolerances are deemed to comply relative to either face, but not to both.

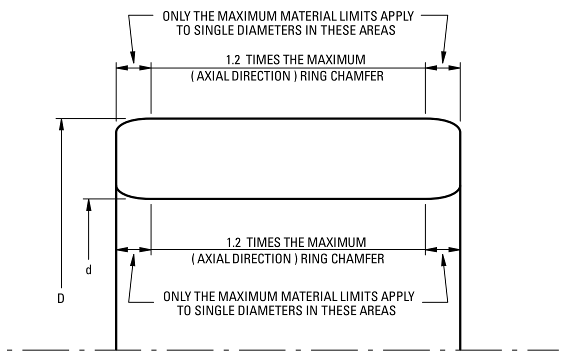
Outer ring flange back face: That side of an outer ring flange that is intended to support axial load.

Middle of raceway: Point or line on a raceway surface halfway between the two edges of the raceway.

Raceway contact diameter: Diameter of the theoretical circle through the nominal points of contact between the rolling elements and the raceway.

NOTE: For roller bearings, the nominal point of contact is generally at the middle of the roller.

Diameter deviation near ring faces: In radial planes, when nearer to the face of a ring than 1.2 times the maximum (axial direction) ring chamfer, only the maximum material limits apply.



ABMA / ISO Symbols - Inner Ring

Δd_{mp} Single plane mean bore diameter deviation from basic bore diameter, e.g., bore tolerance for a basically tapered bore, Δd_{mp} refers only to the theoretical small bore end of the bore.

V_{dsp} Difference between the largest and the smallest of the single bore diameters in a single radial plane.

V_{dmp} Difference between the largest and smallest of the mean bore diameters in a single radial plane of an individual ring.

ABMA / ISO Symbols - Outer Ring

ΔD_{mp} Single plane mean outside diameter deviation from basic outside diameter, e.g., O.D. tolerance.

V_{Dsp} Difference between the largest and smallest of the single outside diameters in a single radial plane.

ENGINEERING

The following tables provide standard ISO tolerance information. They are provided for general use and are referenced throughout this catalog.

ISO Tolerances for Holes – Metric

Diameters **mm**		Deviations **mm**						Deviations **mm**					
		B10		B11		B12		C9		C10		C11	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
3	6	0.188	0.140	0.215	0.140	0.260	0.140	0.100	0.070	0.118	0.070	0.145	0.070
6	10	0.208	0.150	0.240	0.150	0.300	0.150	0.116	0.080	0.138	0.080	0.170	0.080
10	18	0.220	0.150	0.260	0.150	0.330	0.150	0.138	0.095	0.165	0.095	0.205	0.095
18	30	0.244	0.160	0.290	0.160	0.370	0.160	0.162	0.110	0.194	0.110	0.240	0.110
30	40	0.270	0.170	0.330	0.170	0.420	0.170	0.182	0.120	0.220	0.120	0.280	0.120
40	50	0.280	0.180	0.340	0.180	0.430	0.180	0.192	0.130	0.230	0.130	0.290	0.130
50	65	0.310	0.190	0.380	0.190	0.490	0.190	0.214	0.140	0.260	0.140	0.330	0.140
65	80	0.320	0.200	0.390	0.200	0.500	0.200	0.224	0.150	0.270	0.150	0.340	0.150
80	100	0.360	0.220	0.440	0.220	0.570	0.220	0.257	0.170	0.310	0.170	0.390	0.170
100	120	0.380	0.240	0.460	0.240	0.590	0.240	0.267	0.180	0.320	0.180	0.400	0.180
120	140	0.420	0.260	0.510	0.260	0.660	0.260	0.300	0.200	0.360	0.200	0.450	0.200
140	160	0.440	0.280	0.530	0.280	0.680	0.280	0.310	0.210	0.370	0.210	0.460	0.210
160	180	0.470	0.310	0.560	0.310	0.710	0.310	0.330	0.230	0.390	0.230	0.480	0.230
180	200	0.525	0.340	0.630	0.340	0.800	0.340	0.355	0.240	0.425	0.240	0.530	0.240
200	225	0.565	0.380	0.670	0.380	0.840	0.380	0.375	0.260	0.445	0.260	0.550	0.260
225	250	0.605	0.420	0.710	0.420	0.880	0.420	0.395	0.280	0.465	0.280	0.570	0.280
250	280	0.690	0.480	0.800	0.480	1.000	0.480	0.430	0.300	0.510	0.300	0.620	0.300
280	315	0.750	0.540	0.860	0.540	1.060	0.540	0.460	0.330	0.540	0.330	0.650	0.330
315	355	0.830	0.600	0.960	0.600	1.170	0.600	0.500	0.360	0.590	0.360	0.720	0.360
355	400	0.910	0.680	1.040	0.680	1.250	0.680	0.540	0.400	0.630	0.400	0.760	0.400
400	450	1.010	0.760	1.160	0.760	1.390	0.760	0.595	0.440	0.690	0.440	0.840	0.440
450	500	1.090	0.840	1.240	0.840	1.470	0.840	0.635	0.480	0.730	0.480	0.880	0.480

Diameters **mm**		Deviations **mm**									
		E9		E10		E11		E12		E13	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
3	6	0.050	0.020	0.068	0.020	0.095	0.020	0.140	0.020	0.200	0.020
6	10	0.061	0.025	0.083	0.025	0.115	0.025	0.175	0.025	0.245	0.025
10	18	0.075	0.032	0.102	0.032	0.142	0.032	0.212	0.032	0.302	0.032
18	30	0.092	0.040	0.124	0.040	0.170	0.040	0.250	0.040	0.370	0.040
30	50	0.112	0.050	0.150	0.050	0.210	0.050	0.300	0.050	0.440	0.050
50	80	0.134	0.060	0.180	0.060	0.250	0.060	0.360	0.060	0.520	0.060
80	120	0.159	0.072	0.212	0.072	0.292	0.072	0.422	0.072	0.612	0.072
120	180	0.185	0.085	0.245	0.085	0.335	0.085	0.485	0.085	0.715	0.085
180	250	0.215	0.100	0.285	0.100	0.390	0.100	0.560	0.100	0.820	0.100
250	315	0.240	0.110	0.320	0.110	0.430	0.110	0.630	0.110	0.920	0.110
315	400	0.265	0.125	0.355	0.125	0.485	0.125	0.695	0.125	1.015	0.125
400	500	0.290	0.135	0.385	0.135	0.535	0.135	0.765	0.135	1.105	0.135

Diameters **mm**		Deviations **mm**							
		F5		F6		F7		F8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
3	6	0.015	0.010	0.018	0.010	0.022	0.010	0.028	0.010
6	10	0.019	0.013	0.022	0.013	0.028	0.013	0.035	0.013
10	18	0.024	0.016	0.027	0.016	0.034	0.016	0.043	0.016
18	30	0.029	0.020	0.033	0.020	0.041	0.020	0.053	0.020
30	50	0.036	0.025	0.041	0.025	0.050	0.025	0.064	0.025
50	80	0.043	0.030	0.049	0.030	0.060	0.030	0.076	0.030
80	120	0.051	0.036	0.058	0.036	0.071	0.036	0.090	0.036
120	180	0.061	0.043	0.068	0.043	0.083	0.043	0.106	0.043
180	250	0.070	0.050	0.079	0.050	0.096	0.050	0.122	0.050
250	315	0.079	0.056	0.088	0.056	0.108	0.056	0.137	0.056
315	400	0.087	0.062	0.098	0.062	0.119	0.062	0.151	0.062
400	500	0.095	0.068	0.108	0.068	0.131	0.068	0.165	0.068

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Diameter **mm**		Deviations **mm**					
		G5		G6		G7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.
3	6	0.009	0.004	0.012	0.004	0.016	0.004
6	10	0.011	0.005	0.014	0.005	0.020	0.005
10	18	0.014	0.006	0.017	0.006	0.024	0.006
18	30	0.016	0.007	0.020	0.007	0.028	0.007
30	50	0.020	0.009	0.025	0.009	0.034	0.009
50	80	0.023	0.010	0.029	0.010	0.040	0.010
80	120	0.027	0.012	0.034	0.012	0.047	0.012
120	180	0.032	0.014	0.039	0.014	0.054	0.014
180	250	0.035	0.015	0.044	0.015	0.061	0.015
250	315	0.040	0.017	0.049	0.017	0.069	0.017
315	400	0.043	0.018	0.054	0.018	0.075	0.018
400	500	0.047	0.020	0.060	0.020	0.083	0.020

Diameters **mm**		Deviations **mm**									
		H4		H5		H6		H7		H8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
3	6	0.004	0.000	0.005	0.000	0.008	0.000	0.012	0.000	0.018	0.000
6	10	0.004	0.000	0.006	0.000	0.009	0.000	0.015	0.000	0.022	0.000
10	18	0.005	0.000	0.008	0.000	0.011	0.000	0.018	0.000	0.027	0.000
18	30	0.006	0.000	0.009	0.000	0.013	0.000	0.021	0.000	0.033	0.000
30	50	0.007	0.000	0.011	0.000	0.016	0.000	0.025	0.000	0.039	0.000
50	80	0.008	0.000	0.013	0.000	0.019	0.000	0.030	0.000	0.046	0.000
80	120	0.010	0.000	0.015	0.000	0.022	0.000	0.035	0.000	0.054	0.000
120	180	0.012	0.000	0.018	0.000	0.025	0.000	0.040	0.000	0.063	0.000
180	250	0.014	0.000	0.020	0.000	0.029	0.000	0.046	0.000	0.072	0.000
250	315	0.016	0.000	0.023	0.000	0.032	0.000	0.052	0.000	0.081	0.000
315	400	0.018	0.000	0.025	0.000	0.036	0.000	0.057	0.000	0.089	0.000
400	500	0.020	0.000	0.027	0.000	0.040	0.000	0.063	0.000	0.097	0.000

Diameters **mm**		Deviations **mm**							
		H9		H10		H11		H12	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
3	6	0.030	0.000	0.048	0.000	0.075	0.000	0.120	0.000
6	10	0.036	0.000	0.058	0.000	0.090	0.000	0.150	0.000
10	18	0.043	0.000	0.070	0.000	0.110	0.000	0.180	0.000
18	30	0.052	0.000	0.084	0.000	0.130	0.000	0.210	0.000
30	50	0.062	0.000	0.100	0.000	0.160	0.000	0.250	0.000
50	80	0.074	0.000	0.120	0.000	0.190	0.000	0.300	0.000
80	120	0.087	0.000	0.140	0.000	0.220	0.000	0.350	0.000
120	180	0.100	0.000	0.160	0.000	0.250	0.000	0.400	0.000
180	250	0.115	0.000	0.185	0.000	0.290	0.000	0.460	0.000
250	315	0.130	0.000	0.210	0.000	0.320	0.000	0.520	0.000
315	400	0.140	0.000	0.230	0.000	0.360	0.000	0.570	0.000
400	500	0.155	0.000	0.250	0.000	0.400	0.000	0.630	0.000

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Diameters mm		Deviations mm						Deviations mm					
		J6		J7		J8		K6		K7		K8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
3	6	0.005	-0.003	0.006	-0.006	0.010	-0.008	0.002	-0.006	0.003	-0.009	0.005	-0.013
6	10	0.005	-0.004	0.008	-0.007	0.012	-0.010	0.002	-0.007	0.005	-0.010	0.006	-0.016
10	18	0.006	-0.005	0.010	-0.008	0.015	-0.012	0.002	-0.009	0.006	-0.012	0.008	-0.019
18	30	0.008	-0.005	0.012	-0.009	0.020	-0.013	0.002	-0.011	0.006	-0.015	0.010	-0.023
30	50	0.010	-0.006	0.014	-0.011	0.024	-0.015	0.003	-0.013	0.007	-0.018	0.012	-0.027
50	80	0.013	-0.006	0.018	-0.012	0.028	-0.018	0.004	-0.015	0.009	-0.021	0.014	-0.032
80	120	0.016	-0.006	0.022	-0.013	0.034	-0.020	0.004	-0.018	0.010	-0.025	0.016	-0.038
120	180	0.018	-0.007	0.026	-0.014	0.041	-0.022	0.004	-0.021	0.012	-0.028	0.020	-0.043
180	250	0.022	-0.007	0.030	-0.016	0.047	-0.025	0.005	-0.024	0.013	-0.033	0.022	-0.050
250	315	0.025	-0.007	0.036	-0.016	0.055	-0.026	0.005	-0.027	0.016	-0.036	0.025	-0.056
315	400	0.029	-0.007	0.039	-0.018	0.060	-0.029	0.007	-0.029	0.017	-0.040	0.028	-0.061
400	500	0.033	-0.007	0.043	-0.020	0.066	-0.031	0.008	-0.032	0.018	-0.045	0.029	-0.068

Diameters mm		Deviations mm						Deviations mm					
		M5		M6		M7		N6		N7		N8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
3	6	-0.003	-0.008	-0.001	-0.009	0.000	-0.012	-0.005	-0.013	-0.004	-0.016	-0.002	-0.020
6	10	-0.004	-0.010	-0.003	-0.012	0.000	-0.015	-0.007	-0.016	-0.004	-0.019	-0.003	-0.025
10	18	-0.004	-0.012	-0.004	-0.015	0.000	-0.018	-0.009	-0.020	-0.005	-0.023	-0.003	-0.030
18	30	-0.005	-0.014	-0.004	-0.017	0.000	-0.021	-0.011	-0.024	-0.007	-0.028	-0.003	-0.036
30	50	-0.005	-0.016	-0.004	-0.020	0.000	-0.025	-0.012	-0.028	-0.008	-0.033	-0.003	-0.042
50	80	-0.006	-0.019	-0.005	-0.024	0.000	-0.030	-0.014	-0.033	-0.009	-0.039	-0.004	-0.050
80	120	-0.008	-0.023	-0.006	-0.028	0.000	-0.035	-0.016	-0.038	-0.010	-0.045	-0.004	-0.058
120	180	-0.009	-0.027	-0.008	-0.033	0.000	-0.040	-0.020	-0.045	-0.012	-0.052	-0.004	-0.067
180	250	-0.011	-0.031	-0.008	-0.037	0.000	-0.046	-0.022	-0.051	-0.014	-0.060	-0.005	-0.077
250	315	-0.013	-0.036	-0.009	-0.041	0.000	-0.052	-0.025	-0.057	-0.014	-0.066	-0.005	-0.086
315	400	-0.014	-0.039	-0.010	-0.046	0.000	-0.057	-0.026	-0.062	-0.016	-0.073	-0.005	-0.094
400	500	-0.016	-0.043	-0.010	-0.050	0.000	-0.063	-0.027	-0.067	-0.017	-0.080	-0.006	-0.103

Diameters mm		Deviations mm				Deviations mm					
		P6		P7		R6		R7		R8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
3	6	-0.009	-0.017	-0.008	-0.020	-0.012	-0.020	-0.011	-0.023	-0.015	-0.033
6	10	-0.012	-0.021	-0.009	-0.024	-0.016	-0.025	-0.013	-0.028	-0.019	-0.041
10	18	-0.015	-0.026	-0.011	-0.029	-0.020	-0.031	-0.016	-0.034	-0.023	-0.050
18	30	-0.018	-0.031	-0.014	-0.035	-0.024	-0.037	-0.020	-0.041	-0.028	-0.061
30	50	-0.021	-0.037	-0.017	-0.042	-0.029	-0.045	-0.025	-0.050	-0.034	-0.073
50	65	-0.026	-0.045	-0.021	-0.051	-0.035	-0.054	-0.030	-0.060	-0.041	-0.087
65	80	-0.026	-0.045	-0.021	-0.051	-0.037	-0.056	-0.032	-0.062	-0.043	-0.089
80	100	-0.030	-0.052	-0.024	-0.059	-0.044	-0.066	-0.038	-0.073	-0.051	-0.105
100	120	-0.030	-0.052	-0.024	-0.059	-0.047	-0.069	-0.041	-0.076	-0.054	-0.108
120	140	-0.037	-0.061	-0.028	-0.068	-0.056	-0.081	-0.048	-0.088	-0.063	-0.126
140	160	-0.036	-0.061	-0.028	-0.068	-0.058	-0.083	-0.050	-0.090	-0.065	-0.128
160	180	-0.036	-0.061	-0.028	-0.068	-0.061	-0.086	-0.053	-0.093	-0.068	-0.131
180	200	-0.041	-0.070	-0.033	-0.079	-0.068	-0.097	-0.060	-0.106	-0.077	-0.149
200	225	-0.041	-0.070	-0.033	-0.079	-0.071	-0.100	-0.063	-0.109	-0.080	-0.152
225	250	-0.041	-0.070	-0.033	-0.079	-0.075	-0.104	-0.067	-0.113	-0.084	-0.156
250	280	-0.047	-0.079	-0.036	-0.088	-0.085	-0.117	-0.074	-0.126	-0.094	-0.175
280	315	-0.047	-0.079	-0.036	-0.088	-0.089	-0.121	-0.078	-0.130	-0.098	-0.179
315	355	-0.051	-0.087	-0.041	-0.098	-0.097	-0.133	-0.087	-0.144	-0.108	-0.197
355	400	-0.051	-0.087	-0.041	-0.098	-0.103	-0.139	-0.093	-0.150	-0.114	-0.203
400	450	-0.055	-0.095	-0.045	-0.108	-0.113	-0.153	-0.103	-0.166	-0.126	-0.223
450	500	-0.055	-0.095	-0.045	-0.108	-0.119	-0.159	-0.109	-0.172	-0.132	-0.229

ISO Tolerances for Shafts – Metric

Diameters **mm**		Deviations **mm**							
		a10		a11		a12		a13	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	3	-0.270	-0.310	-0.270	-0.330	-0.270	-0.370	-0.270	-0.410
3	6	-0.270	-0.318	-0.270	-0.345	-0.270	-0.390	-0.270	-0.450
6	10	-0.280	-0.338	-0.280	-0.370	-0.280	-0.430	-0.280	-0.500
10	18	-0.290	-0.360	-0.290	-0.400	-0.290	-0.470	-0.290	-0.560
18	30	-0.300	-0.384	-0.300	-0.430	-0.300	-0.510	-0.300	-0.630
30	40	-0.310	-0.410	-0.310	-0.470	-0.310	-0.560	-0.310	-0.700
40	50	-0.320	-0.420	-0.320	-0.480	-0.320	-0.570	-0.320	-0.710
50	65	-0.340	-0.460	-0.340	-0.530	-0.340	-0.640	-0.340	-0.800
65	80	-0.360	-0.480	-0.360	-0.550	-0.360	-0.660	-0.360	-0.820
80	100	-0.380	-0.520	-0.380	-0.600	-0.380	-0.730	-0.380	-0.920
100	120	-0.410	-0.550	-0.410	-0.630	-0.410	-0.760	-0.410	-0.950
120	140	-0.460	-0.620	-0.460	-0.710	-0.460	-0.860	-0.460	-1.090
140	160	-0.520	-0.680	-0.520	-0.770	-0.520	-0.920	-0.520	-1.150
160	180	-0.580	-0.740	-0.580	-0.830	-0.580	-0.980	-0.580	-1.210
180	200	-0.660	-0.845	-0.660	-0.950	-0.660	-1.120	-0.660	-1.380
200	225	-0.740	-0.925	-0.740	-1.030	-0.740	-1.200	-0.740	-1.460
225	250	-0.820	-1.005	-0.820	-1.110	-0.820	-1.280	-0.820	-1.540
250	280	-0.920	-1.130	-0.920	-1.240	-0.920	-1.440	-0.920	-1.730
280	315	-1.050	-1.260	-1.050	-1.370	-1.050	-1.570	-1.050	-1.860
315	355	-1.200	-1.430	-1.200	-1.560	-1.200	-1.770	-1.200	-2.090
355	400	-1.350	-1.580	-1.350	-1.710	-1.350	-1.920	-1.350	-2.240

Diameters **mm**		Deviations **mm**						Deviations **mm**					
		c11		c12		c13		e11		e12		e13	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	3	-0.060	-0.120	-0.060	-0.160	-0.060	-0.200	-0.014	-0.074	-0.014	-0.114	-0.014	-0.154
3	6	-0.070	-0.145	-0.070	-0.190	-0.070	-0.250	-0.020	-0.095	-0.020	-0.140	-0.020	-0.200
6	10	-0.080	-0.170	-0.080	-0.230	-0.080	-0.300	-0.025	-0.115	-0.025	-0.175	-0.025	-0.245
10	18	-0.095	-0.205	-0.095	-0.275	-0.095	-0.365	-0.032	-0.142	-0.032	-0.212	-0.032	-0.302
18	30	-0.110	-0.240	-0.110	-0.320	-0.110	-0.440	-0.040	-0.170	-0.040	-0.250	-0.040	-0.370
30	40	-0.120	-0.280	-0.120	-0.370	-0.120	-0.510	-0.050	-0.210	-0.050	-0.300	-0.050	-0.440
40	50	-0.130	-0.290	-0.130	-0.380	-0.130	-0.520	-0.050	-0.210	-0.050	-0.300	-0.050	-0.440
50	65	-0.140	-0.330	-0.140	-0.440	-0.140	-0.600	-0.060	-0.250	-0.060	-0.360	-0.060	-0.520
65	80	-0.150	-0.340	-0.150	-0.450	-0.150	-0.610	-0.060	-0.250	-0.060	-0.360	-0.060	-0.520
80	100	-0.170	-0.390	-0.170	-0.520	-0.170	-0.710	-0.072	-0.292	-0.072	-0.422	-0.072	-0.612
100	120	-0.180	-0.400	-0.180	-0.530	-0.180	-0.720	-0.072	-0.292	-0.072	-0.422	-0.072	-0.612
120	140	-0.200	-0.450	-0.200	-0.600	-0.200	-0.830	-0.085	-0.335	-0.085	-0.485	-0.085	-0.715
140	160	-0.210	-0.460	-0.210	-0.610	-0.210	-0.840	-0.085	-0.335	-0.085	-0.485	-0.085	-0.715
160	180	-0.230	-0.480	-0.230	-0.630	-0.230	-0.860	-0.085	-0.335	-0.085	-0.485	-0.085	-0.715
180	200	-0.240	-0.530	-0.240	-0.700	-0.240	-0.960	-0.100	-0.390	-0.100	-0.560	-0.100	-0.820
200	225	-0.260	-0.550	-0.260	-0.720	-0.260	-0.980	-0.100	-0.390	-0.100	-0.560	-0.100	-0.820
225	250	-0.280	-0.570	-0.280	-0.740	-0.280	-1.000	-0.100	-0.390	-0.100	-0.560	-0.100	-0.820
250	280	-0.300	-0.620	-0.300	-0.820	-0.300	-1.110	-0.110	-0.430	-0.110	-0.630	-0.110	-0.920
280	315	-0.330	-0.650	-0.330	-0.850	-0.330	-1.140	-0.110	-0.430	-0.110	-0.630	-0.110	-0.920
315	355	-0.360	-0.720	-0.360	-0.930	-0.360	-1.250	-0.125	-0.485	-0.125	-0.695	-0.125	-1.015
355	400	-0.400	-0.760	-0.400	-0.970	-0.400	-1.290	-0.125	-0.485	-0.125	-0.695	-0.125	-1.015

ENGINEERING

ISO Tolerances for Shafts – Metric

Diameters **mm**		Deviations **mm**						Deviations **mm**					
		f5		f6		f7		g5		g6		g7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	3	-0.006	-0.010	-0.006	-0.012	-0.006	-0.016	-0.002	-0.006	-0.002	-0.008	-0.002	-0.012
3	6	-0.010	-0.015	-0.010	-0.018	-0.010	-0.022	-0.004	-0.009	-0.004	-0.012	-0.004	-0.016
6	10	-0.013	-0.019	-0.013	-0.022	-0.013	-0.028	-0.005	-0.011	-0.005	-0.014	-0.005	-0.020
10	18	-0.016	-0.024	-0.016	-0.027	-0.016	-0.034	-0.006	-0.014	-0.006	-0.017	-0.006	-0.024
18	30	-0.020	-0.029	-0.020	-0.033	-0.020	-0.041	-0.007	-0.016	-0.007	-0.020	-0.007	-0.028
30	50	-0.025	-0.036	-0.025	-0.041	-0.025	-0.050	-0.009	-0.020	-0.009	-0.025	-0.009	-0.034
50	80	-0.030	-0.043	-0.030	-0.049	-0.030	-0.060	-0.010	-0.023	-0.010	-0.029	-0.010	-0.040
80	120	-0.036	-0.051	-0.036	-0.058	-0.036	-0.071	-0.012	-0.027	-0.012	-0.034	-0.012	-0.047
120	180	-0.043	-0.061	-0.043	-0.068	-0.043	-0.083	-0.014	-0.032	-0.014	-0.039	-0.014	-0.054
180	250	-0.050	-0.070	-0.050	-0.079	-0.050	-0.096	-0.015	-0.035	-0.015	-0.044	-0.015	-0.061
250	315	-0.056	-0.079	-0.056	-0.088	-0.056	-0.108	-0.017	-0.040	-0.017	-0.049	-0.017	-0.069
315	400	-0.062	-0.087	-0.062	-0.098	-0.062	-0.119	-0.018	-0.043	-0.018	-0.054	-0.018	-0.075

Diameters **mm**		Deviations **mm**									
		h4		h5		h6		h7		h8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	3	0.000	-0.003	0.000	-0.004	0.000	-0.006	0.000	-0.010	0.000	-0.014
3	6	0.000	-0.004	0.000	-0.005	0.000	-0.008	0.000	-0.012	0.000	-0.018
6	10	0.000	-0.004	0.000	-0.006	0.000	-0.009	0.000	-0.015	0.000	-0.022
10	18	0.000	-0.005	0.000	-0.008	0.000	-0.011	0.000	-0.018	0.000	-0.027
18	30	0.000	-0.006	0.000	-0.009	0.000	-0.013	0.000	-0.021	0.000	-0.033
30	50	0.000	-0.007	0.000	-0.011	0.000	-0.016	0.000	-0.025	0.000	-0.039
50	80	0.000	-0.008	0.000	-0.013	0.000	-0.019	0.000	-0.030	0.000	-0.046
80	120	0.000	-0.010	0.000	-0.015	0.000	-0.022	0.000	-0.035	0.000	-0.054
120	180	0.000	-0.012	0.000	-0.018	0.000	-0.025	0.000	-0.040	0.000	-0.063
180	250	0.000	-0.014	0.000	-0.020	0.000	-0.029	0.000	-0.046	0.000	-0.072
250	315	0.000	-0.016	0.000	-0.023	0.000	-0.032	0.000	-0.052	0.000	-0.081
315	400	0.000	-0.018	0.000	-0.025	0.000	-0.036	0.000	-0.057	0.000	-0.089

Diameters **mm**		Deviations **mm**									
		h9		h10		h11		h12		h13	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	3	0.000	-0.025	0.000	-0.040	0.000	-0.060	0.000	-0.100	0.000	-0.140
3	6	0.000	-0.030	0.000	-0.048	0.000	-0.075	0.000	-0.120	0.000	-0.180
6	10	0.000	-0.036	0.000	-0.058	0.000	-0.090	0.000	-0.150	0.000	-0.220
10	18	0.000	-0.043	0.000	-0.070	0.000	-0.110	0.000	-0.180	0.000	-0.270
18	30	0.000	-0.052	0.000	-0.084	0.000	-0.130	0.000	-0.210	0.000	-0.330
30	50	0.000	-0.062	0.000	-0.100	0.000	-0.160	0.000	-0.250	0.000	-0.390
50	80	0.000	-0.074	0.000	-0.120	0.000	-0.190	0.000	-0.300	0.000	-0.460
80	120	0.000	-0.087	0.000	-0.140	0.000	-0.220	0.000	-0.350	0.000	-0.540
120	180	0.000	-0.100	0.000	-0.160	0.000	-0.250	0.000	-0.400	0.000	-0.630
180	250	0.000	-0.115	0.000	-0.185	0.000	-0.290	0.000	-0.460	0.000	-0.720
250	315	0.000	-0.130	0.000	-0.210	0.000	-0.320	0.000	-0.520	0.000	-0.810
315	400	0.000	-0.140	0.000	-0.230	0.000	-0.360	0.000	-0.570	0.000	-0.890

ISO Tolerances for Shafts – Metric													
Diameter **mm**		Deviations **mm**						Deviations **mm**					
		j5		j6		j7		k5		k6		k7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	3	0.002	-0.002	0.004	-0.002	0.006	-0.004	0.004	0.000	0.006	0.000	0.010	0.000
3	6	0.003	-0.002	0.006	-0.002	0.008	-0.004	0.006	0.001	0.009	0.001	0.013	0.001
6	10	0.004	-0.002	0.007	-0.002	0.010	-0.005	0.007	0.001	0.010	0.001	0.016	0.001
10	18	0.005	-0.003	0.008	-0.003	0.012	-0.006	0.009	0.001	0.012	0.001	0.019	0.001
18	30	0.005	-0.004	0.009	-0.004	0.013	-0.008	0.011	0.002	0.015	0.002	0.023	0.002
30	50	0.006	-0.005	0.011	-0.005	0.015	-0.010	0.013	0.002	0.018	0.002	0.027	0.002
50	80	0.006	-0.007	0.012	-0.007	0.018	-0.012	0.015	0.002	0.021	0.002	0.032	0.002
80	120	0.006	-0.009	0.013	-0.009	0.020	-0.015	0.018	0.003	0.025	0.003	0.038	0.003
120	180	0.007	-0.011	0.014	-0.011	0.022	-0.018	0.021	0.003	0.028	0.003	0.043	0.003
180	250	0.007	-0.013	0.016	-0.013	0.025	-0.021	0.024	0.004	0.033	0.004	0.050	0.004
250	315	0.007	-0.016	0.016	-0.016	0.026	-0.026	0.027	0.004	0.036	0.004	0.056	0.004
315	400	0.007	-0.018	0.018	-0.018	0.029	-0.028	0.029	0.004	0.040	0.004	0.061	0.004

Diameter **mm**		Deviations **mm**						Deviations **mm**					
		m5		m6		m7		n5		n6		n7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	3	0.006	0.002	0.008	0.002	0.012	0.002	0.008	0.004	0.010	0.004	0.014	0.004
3	6	0.009	0.004	0.012	0.004	0.016	0.004	0.013	0.008	0.016	0.008	0.020	0.008
6	10	0.012	0.006	0.015	0.006	0.021	0.006	0.016	0.010	0.019	0.010	0.025	0.010
10	18	0.015	0.007	0.018	0.007	0.025	0.007	0.020	0.012	0.023	0.012	0.030	0.012
18	30	0.017	0.008	0.021	0.008	0.029	0.008	0.024	0.015	0.028	0.015	0.036	0.015
30	50	0.020	0.009	0.025	0.009	0.034	0.009	0.028	0.017	0.033	0.017	0.042	0.017
50	80	0.024	0.011	0.030	0.011	0.041	0.011	0.033	0.020	0.039	0.020	0.050	0.020
80	120	0.028	0.013	0.035	0.013	0.048	0.013	0.038	0.023	0.045	0.023	0.058	0.023
120	180	0.033	0.015	0.040	0.015	0.055	0.015	0.045	0.027	0.052	0.027	0.067	0.027
180	250	0.037	0.017	0.046	0.017	0.063	0.017	0.051	0.031	0.060	0.031	0.077	0.031
250	315	0.043	0.020	0.052	0.020	0.072	0.020	0.057	0.034	0.066	0.034	0.086	0.034
315	400	0.046	0.021	0.057	0.021	0.078	0.021	0.062	0.037	0.073	0.037	0.094	0.037

Diameter **mm**		Deviations **mm**					
		p6		r6		r7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.
80	100	0.059	0.037	-	-	-	-
100	120	0.059	0.037	-	-	-	-
120	140	0.068	0.043	0.090	0.065	-	-
140	160	0.068	0.043	0.090	0.065	-	-
160	180	0.068	0.043	0.090	0.065	-	-
180	200	0.079	0.050	0.106	0.077	-	-
200	225	0.079	0.050	0.109	0.080	0.126	0.080
225	250	0.079	0.050	0.113	0.084	0.130	0.084
250	280	0.088	0.056	0.126	0.094	0.146	0.094
280	315	0.088	0.056	0.130	0.098	0.150	0.098
315	355	0.098	0.062	0.144	0.108	0.165	0.108
355	400	0.098	0.062	0.150	0.114	0.171	0.114
400	450	0.108	0.068	0.166	0.126	0.189	0.126
450	500	0.108	0.068	0.172	0.132	0.195	0.132

ENGINEERING

ISO Tolerances for Holes – inch

Diameter in		Deviations in						Deviations in					
		B10		B11		B12		C9		C10		C11	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
0.1181	0.2362	+0.0074	+0.0055	+0.0085	+0.0055	+0.0102	+0.0055	+0.0039	+0.0028	+0.0046	+0.0028	+0.0057	+0.0028
0.2362	0.3937	+0.0082	+0.0059	+0.0094	+0.0059	+0.0118	+0.0059	+0.0046	+0.0031	+0.0054	+0.0031	+0.0067	+0.0031
0.3937	0.7087	+0.0087	+0.0059	+0.0102	+0.0059	+0.0130	+0.0059	+0.0054	+0.0037	+0.0065	+0.0037	+0.0081	+0.0037
0.7087	1.1811	+0.0096	+0.0063	+0.0114	+0.0063	+0.0146	+0.0063	+0.0064	+0.0043	+0.0076	+0.0043	+0.0094	+0.0043
1.1811	1.5748	+0.0106	+0.0067	+0.0130	+0.0067	+0.0165	+0.0067	+0.0072	+0.0047	+0.0087	+0.0047	+0.0110	+0.0047
1.5748	1.9685	+0.0110	+0.0071	+0.0134	+0.0071	+0.0169	+0.0071	+0.0076	+0.0051	+0.0091	+0.0051	+0.0114	+0.0051
1.9685	2.5591	+0.0122	+0.0075	+0.0150	+0.0075	+0.0193	+0.0075	+0.0084	+0.0055	+0.0102	+0.0055	+0.0120	+0.0055
2.5591	3.1496	+0.0126	+0.0079	+0.0154	+0.0079	+0.0197	+0.0079	+0.0088	+0.0059	+0.0106	+0.0059	+0.0134	+0.0059
3.1496	3.9370	+0.0142	+0.0087	+0.0173	+0.0087	+0.0224	+0.0087	+0.0101	+0.0067	+0.0122	+0.0067	+0.0154	+0.0067
3.9370	4.7244	+0.0150	+0.0094	+0.0181	+0.0094	+0.0232	+0.0094	+0.0105	+0.0071	+0.0126	+0.0071	+0.0157	+0.0071
4.7244	5.5118	+0.0165	+0.0102	+0.0201	+0.0102	+0.0260	+0.0102	+0.0118	+0.0079	+0.0142	+0.0079	+0.0177	+0.0079
5.5118	6.2992	+0.0173	+0.0110	+0.0209	+0.0110	+0.0268	+0.0110	+0.0122	+0.0083	+0.0146	+0.0083	+0.0181	+0.0083
6.2992	7.0866	+0.0185	+0.0122	+0.0220	+0.0122	+0.0280	+0.0122	+0.0130	+0.0091	+0.0154	+0.0091	+0.0189	+0.0091
7.0866	7.8740	+0.0207	+0.0134	+0.0248	+0.0134	+0.0315	+0.0134	+0.0140	+0.0094	+0.0167	+0.0094	+0.0209	+0.0094
7.8740	8.8583	+0.0222	+0.0150	+0.0264	+0.0150	+0.0331	+0.0150	+0.0148	+0.0102	+0.0175	+0.0102	+0.0217	+0.0102
8.8583	9.8425	+0.0238	+0.0165	+0.0280	+0.0165	+0.0346	+0.0165	+0.0156	+0.0110	+0.0183	+0.0110	+0.0224	+0.0110
9.8425	11.0236	+0.0272	+0.0189	+0.0315	+0.0189	+0.0394	+0.0189	+0.0169	+0.0118	+0.0201	+0.0118	+0.0244	+0.0118
11.0236	12.4016	+0.0295	+0.0213	+0.0339	+0.0213	+0.0417	+0.0213	+0.0181	+0.0130	+0.0213	+0.0130	+0.0256	+0.0130
12.4016	13.9764	+0.0327	+0.0236	+0.0378	+0.0236	+0.0461	+0.0236	+0.0197	+0.0142	+0.0232	+0.0142	+0.0283	+0.0142
13.9764	15.7480	+0.0358	+0.0268	+0.0409	+0.0268	+0.0492	+0.0268	+0.0213	+0.0157	+0.0248	+0.0157	+0.0299	+0.0157
15.7480	17.7165	+0.0398	+0.0299	+0.0457	+0.0299	+0.0547	+0.0299	+0.0234	+0.0173	+0.0272	+0.0173	+0.0331	+0.0173
17.71654	19.6850	+0.0429	+0.0331	+0.0488	+0.0331	+0.0579	+0.0331	+0.0250	+0.0189	+0.0287	+0.0189	+0.0346	+0.0189

Diameter in		Deviations in									
		E9		E10		E11		E12		E13	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
0.1181	0.2362	+0.0020	+0.0008	+0.0027	+0.0008	+0.0037	+0.0008	+0.0055	+0.0008	+0.0079	+0.0008
0.2362	0.3937	+0.0024	+0.0010	+0.0033	+0.0010	+0.0045	+0.0010	+0.0069	+0.0010	+0.0096	+0.0010
0.3937	0.7087	+0.0030	+0.0013	+0.0040	+0.0013	+0.0056	+0.0013	+0.0083	+0.0013	+0.0119	+0.0013
0.7087	1.1811	+0.0036	+0.0016	+0.0049	+0.0016	+0.0067	+0.0016	+0.0098	+0.0016	+0.0146	+0.0016
1.1811	1.9685	+0.0044	+0.0020	+0.0059	+0.0020	+0.0083	+0.0020	+0.0118	+0.0020	+0.0173	+0.0020
1.9685	3.1496	+0.0053	+0.0024	+0.0071	+0.0024	+0.0098	+0.0024	+0.0142	+0.0024	+0.0205	+0.0024
3.1496	4.7244	+0.0063	+0.0028	+0.0083	+0.0028	+0.0115	+0.0028	+0.0166	+0.0028	+0.0241	+0.0028
4.7244	7.0866	+0.0073	+0.0033	+0.0096	+0.0033	+0.0132	+0.0033	+0.0191	+0.0033	+0.0281	+0.0033
7.0866	9.8425	+0.0085	+0.0039	+0.0112	+0.0039	+0.0154	+0.0039	+0.0220	+0.0039	+0.0323	+0.0039
9.8425	12.4016	+0.0094	+0.0043	+0.0126	+0.0043	+0.0169	+0.0043	+0.0248	+0.0043	+0.0362	+0.0043
12.4016	15.7480	+0.0104	+0.0049	+0.0140	+0.0049	+0.0191	+0.0049	+0.0274	+0.0049	+0.0400	+0.0049
15.7480	19.6850	+0.0114	+0.0053	+0.0152	+0.0053	+0.0211	+0.0053	+0.0301	+0.0053	+0.0435	+0.0053

Diameter in		Deviations in							
		F5		F6		F7		F8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
0.1181	0.2362	+0.0006	+0.0004	+0.0007	+0.0004	+0.0009	+0.0004	+0.0011	+0.0004
0.2362	0.3937	+0.0007	+0.0005	+0.0009	+0.0005	+0.0011	+0.0005	+0.0014	+0.0005
0.3937	0.7087	+0.0009	+0.0006	+0.0011	+0.0006	+0.0013	+0.0006	+0.0017	+0.0006
0.7087	1.1811	+0.0011	+0.0008	+0.0013	+0.0008	+0.0016	+0.0008	+0.0021	+0.0008
1.1811	1.9685	+0.0014	+0.0010	+0.0016	+0.0010	+0.0020	+0.0010	+0.0025	+0.0010
1.9685	3.1496	+0.0017	+0.0012	+0.0019	+0.0012	+0.0024	+0.0012	+0.0030	+0.0012
3.1496	4.7244	+0.0020	+0.0014	+0.0023	+0.0014	+0.0028	+0.0014	+0.0035	+0.0014
4.7244	7.0866	+0.0024	+0.0017	+0.0027	+0.0017	+0.0033	+0.0017	+0.0042	+0.0017
7.0866	9.8425	+0.0028	+0.0020	+0.0031	+0.0020	+0.0038	+0.0020	+0.0048	+0.0020
9.8425	12.4016	+0.0031	+0.0022	+0.0035	+0.0022	+0.0043	+0.0022	+0.0054	+0.0022
12.4016	15.7480	+0.0034	+0.0024	+0.0039	+0.0024	+0.0047	+0.0024	+0.0059	+0.0024
15.7480	19.6850	+0.0037	+0.0027	+0.0043	+0.0027	+0.0052	+0.0027	+0.0065	+0.0027

ISO Tolerances for Holes – inch							
Diameter in		Deviations in					
		G5		G6		G7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.
0.1181	0.2362	+0.0004	+0.0002	+0.0005	+0.0002	+0.0006	+0.0002
0.2362	0.3937	+0.0004	+0.0002	+0.0006	+0.0002	+0.0008	+0.0002
0.3937	0.7087	+0.0006	+0.0002	+0.0007	+0.0002	+0.0009	+0.0002
0.7087	1.1811	+0.0006	+0.0003	+0.0008	+0.0003	+0.0011	+0.0003
1.1811	1.9685	+0.0008	+0.0004	+0.0010	+0.0004	+0.0013	+0.0004
1.9685	3.1496	+0.0009	+0.0004	+0.0011	+0.0004	+0.0016	+0.0004
3.1496	4.7244	+0.0011	+0.0005	+0.0013	+0.0005	+0.0019	+0.0005
4.7244	7.0866	+0.0013	+0.0006	+0.0015	+0.0006	+0.0021	+0.0006
7.0866	9.8425	+0.0014	+0.0006	+0.0017	+0.0006	+0.0024	+0.0006
9.8425	12.4016	+0.0016	+0.0007	+0.0019	+0.0007	+0.0027	+0.0007
12.4016	15.7480	+0.0017	+0.0007	+0.0021	+0.0007	+0.0030	+0.0007
15.7480	19.6850	+0.0019	+0.0008	+0.0024	+0.0008	+0.0033	+0.0008

Diameter in		Deviations in									
		H4		H5		H6		H7		H8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
0.1181	0.2362	+0.0002	0	+0.0002	0	+0.0003	0	+0.0005	0	+0.0007	0
0.2362	0.3937	+0.0002	0	+0.0002	0	+0.0004	0	+0.0006	0	+0.0009	0
0.3937	0.7087	+0.0002	0	+0.0003	0	+0.0004	0	+0.0007	0	+0.0011	0
0.7087	1.1811	+0.0002	0	+0.0004	0	+0.0005	0	+0.0008	0	+0.0013	0
1.1811	1.9685	+0.0003	0	+0.0004	0	+0.0006	0	+0.0010	0	+0.0015	0
1.9685	3.1496	+0.0003	0	+0.0005	0	+0.0007	0	+0.0012	0	+0.0018	0
3.1496	4.7244	+0.0004	0	+0.0006	0	+0.0009	0	+0.0014	0	+0.0021	0
4.7244	7.0866	+0.0005	0	+0.0007	0	+0.0010	0	+0.0016	0	+0.0025	0
7.0866	9.8425	+0.0006	0	+0.0008	0	+0.0011	0	+0.0018	0	+0.0028	0
9.8425	12.4016	+0.0006	0	+0.0009	0	+0.0013	0	+0.0020	0	+0.0032	0
12.4016	15.7480	+0.0007	0	+0.0010	0	+0.0014	0	+0.0022	0	+0.0035	0
15.7480	19.6850	+0.0008	0	+0.0011	0	+0.0016	0	+0.0025	0	+0.0038	0

Diameter in		Deviations in							
		H9		H10		H11		H12	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
0.1181	0.2362	+0.0012	0	+0.0019	0	+0.0030	0	+0.0047	0
0.2362	0.3937	+0.0014	0	+0.0023	0	+0.0035	0	+0.0059	0
0.3937	0.7087	+0.0017	0	+0.0028	0	+0.0043	0	+0.0071	0
0.7087	1.1811	+0.0020	0	+0.0033	0	+0.0051	0	+0.0083	0
1.1811	1.9685	+0.0024	0	+0.0039	0	+0.0063	0	+0.0098	0
1.9685	3.1496	+0.0029	0	+0.0047	0	+0.0075	0	+0.0118	0
3.1496	4.7244	+0.0034	0	+0.0055	0	+0.0087	0	+0.0138	0
4.7244	7.0866	+0.0039	0	+0.0063	0	+0.0098	0	+0.0157	0
7.0866	9.8425	+0.0045	0	+0.0073	0	+0.0114	0	+0.0181	0
9.8425	12.4016	+0.0051	0	+0.0083	0	+0.0126	0	+0.0205	0
12.4016	15.7480	+0.0055	0	+0.0091	0	+0.0142	0	+0.0224	0
15.7480	19.6850	+0.0061	0	+0.0098	0	+0.0157	0	+0.0248	0

ENGINEERING

A

ISO Tolerances for Holes – inch

Diameter in		Deviations in						Deviations in					
		J6		J7		J8		K6		K7		K8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
0.1181	0.2362	+0.00020	-0.00012	+0.00024	-0.00024	+0.00039	-0.00031	+0.00008	-0.00024	+0.00012	-0.00035	+0.00020	-0.00051
0.2362	0.3937	+0.00020	-0.00016	+0.00031	-0.00028	+0.00047	-0.00039	+0.00008	-0.00028	+0.00020	-0.00039	+0.00024	-0.00063
0.3937	0.7087	+0.00024	-0.00020	+0.00039	-0.00031	+0.00059	-0.00047	+0.00008	-0.00035	+0.00024	-0.00047	+0.00031	-0.00075
0.7087	1.1811	+0.00031	-0.00020	+0.00047	-0.00035	+0.00079	-0.00051	+0.00008	-0.00043	+0.00024	-0.00059	+0.00039	-0.00091
1.1811	1.9685	+0.00039	-0.00024	+0.00055	-0.00043	+0.00094	-0.00059	+0.00012	-0.00051	+0.00028	-0.00071	+0.00047	-0.00106
1.9685	3.1496	+0.00051	-0.00024	+0.00071	-0.00047	+0.00110	-0.00071	+0.00016	-0.00059	+0.00035	-0.00083	+0.00055	-0.00126
3.1496	4.7244	+0.00063	-0.00024	+0.00087	-0.00051	+0.00134	-0.00079	+0.00016	-0.00071	+0.00039	-0.00098	+0.00063	-0.00150
4.7244	7.0866	+0.00071	-0.00028	+0.00102	-0.00055	+0.00161	-0.00087	+0.00016	-0.00083	+0.00047	-0.00110	+0.00079	-0.00169
7.0866	9.8425	+0.00087	-0.00028	+0.00118	-0.00063	+0.00185	-0.00098	+0.00020	-0.00094	+0.00051	-0.00130	+0.00087	-0.00197
9.8425	12.4016	+0.00098	-0.00028	+0.00142	-0.00063	+0.00217	-0.00102	+0.00020	-0.00106	+0.00063	-0.00142	+0.00098	-0.00220
12.4016	15.7480	+0.00114	-0.00028	+0.00154	-0.00071	+0.00236	-0.00114	+0.00028	-0.00114	+0.00067	-0.00157	+0.00110	-0.00240
15.7480	19.6850	+0.00130	-0.00028	+0.00169	-0.00079	+0.00259	-0.00122	+0.00031	-0.00126	+0.00071	-0.00177	+0.00114	-0.00268

Diameter in		Deviations in						Deviations in					
		M5		M6		M7		N6		N7		N8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
0.1181	0.2362	-0.00012	-0.00031	-0.00004	-0.00035	0	-0.00047	-0.0002	-0.0005	-0.0002	-0.0006	-0.0001	-0.0008
0.2362	0.3937	-0.00016	-0.00039	-0.00012	-0.00047	0	-0.00059	-0.0003	-0.0006	-0.0002	-0.0007	-0.0001	-0.0010
0.3937	0.7087	-0.00016	-0.00047	-0.00016	-0.00059	0	-0.00071	-0.0004	-0.0008	-0.0002	-0.0009	-0.0001	-0.0012
0.7087	1.1811	-0.00020	-0.00055	-0.00016	-0.00067	0	-0.00083	-0.0004	-0.0009	-0.0003	-0.0011	-0.0001	-0.0014
1.1811	1.9685	-0.00020	-0.00063	-0.00016	-0.00079	0	-0.00098	-0.0005	-0.0011	-0.0003	-0.0013	-0.0001	-0.0017
1.9685	3.1496	-0.00024	-0.00075	-0.00020	-0.00094	0	-0.00118	-0.0006	-0.0013	-0.0004	-0.0015	-0.0002	-0.0020
3.1496	4.7244	-0.00031	-0.00091	-0.00024	-0.00110	0	-0.00138	-0.0006	-0.0015	-0.0004	-0.0018	-0.0002	-0.0023
4.7244	7.0866	-0.00035	-0.00106	-0.00031	-0.00130	0	-0.00157	-0.0008	-0.0018	-0.0005	-0.0020	-0.0002	-0.0026
7.0866	9.8425	-0.00043	-0.00122	-0.00031	-0.00146	0	-0.00181	-0.0009	-0.0020	-0.0006	-0.0024	-0.0002	-0.0030
9.8425	12.4016	-0.00051	-0.00142	-0.00035	-0.00161	0	-0.00205	-0.0000	-0.0022	-0.0006	-0.0026	-0.0002	-0.0034
12.4016	15.7480	-0.00055	-0.00154	-0.00039	-0.00181	0	-0.00224	-0.0010	-0.0024	-0.0006	-0.0029	-0.0002	-0.0037
15.7480	19.6850	-0.00063	-0.00169	-0.00039	-0.00197	0	-0.00248	-0.0011	-0.0026	-0.0007	-0.0031	-0.0002	-0.0041

Diameter in		Deviations in				Deviations in					
		P6		P7		R6		R7		R8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
0.1181	0.2362	-0.0004	-0.0007	-0.0003	-0.0008	-0.0005	-0.0008	-0.0004	-0.0009	-0.0006	-0.0013
0.2362	0.3937	-0.0005	-0.0008	-0.0004	-0.0009	-0.0006	-0.0010	-0.0005	-0.0011	-0.0007	-0.0016
0.3937	0.7087	-0.0006	-0.0010	-0.0004	-0.0011	-0.0008	-0.0012	-0.0006	-0.0013	-0.0009	-0.0020
0.7087	1.1811	-0.0007	-0.0012	-0.0006	-0.0014	-0.0009	-0.0015	-0.0008	-0.0016	-0.0011	-0.0024
1.1811	1.9685	-0.0008	-0.0015	-0.0007	-0.0017	-0.0011	-0.0018	-0.0010	-0.0020	-0.0013	-0.0029
1.9685	2.5591	-0.0010	-0.0018	-0.0008	-0.0020	-0.0014	-0.0021	-0.0012	-0.0024	-0.0016	-0.0034
2.5591	3.1496	-0.0010	-0.0018	-0.0008	-0.0020	-0.0015	-0.0022	-0.0013	-0.0024	-0.0017	-0.0035
3.1496	3.9370	-0.0012	-0.0020	-0.0009	-0.0023	-0.0017	-0.0026	-0.0015	-0.0029	-0.0020	-0.0041
3.9370	4.7244	-0.0012	-0.0020	-0.0009	-0.0023	-0.0019	-0.0027	-0.0016	-0.0030	-0.0021	-0.0043
4.7244	5.5118	-0.0014	-0.0024	-0.0011	-0.0027	-0.0022	-0.0032	-0.0019	-0.0035	-0.0025	-0.0050
5.5118	6.2992	-0.0014	-0.0024	-0.0011	-0.0027	-0.0023	-0.0033	-0.0020	-0.0035	-0.0026	-0.0050
6.2992	7.0866	-0.0014	-0.0024	-0.0011	-0.0027	0.0024	-0.0034	-0.0021	-0.0037	-0.0027	-0.0052
7.0866	7.8740	-0.0016	-0.0028	-0.0013	-0.0031	-0.0027	-0.0038	-0.0024	-0.0042	-0.0030	-0.0059
7.8740	8.8583	-0.0016	-0.0028	-0.0013	-0.0031	0.0028	-0.0039	-0.0025	-0.0043	-0.0031	-0.0060
8.8583	9.8425	-0.0016	-0.0028	-0.0013	-0.0031	-0.0030	-0.0041	-0.0026	-0.0044	-0.0033	-0.0061
9.8425	11.0236	-0.0019	-0.0031	-0.0014	-0.0035	-0.0033	-0.0046	-0.0029	-0.0050	-0.0037	-0.0069
11.0236	12.4016	-0.0019	-0.0031	-0.0014	-0.0035	-0.0035	-0.0048	-0.0031	-0.0051	-0.0039	-0.0070
12.4016	13.9764	-0.0020	-0.0034	-0.0016	-0.0039	-0.0038	-0.0052	-0.0034	-0.0057	-0.0043	-0.0078
13.9764	15.7480	-0.0020	-0.0034	-0.0016	-0.0039	-0.0041	-0.0055	-0.0037	-0.0059	-0.0045	-0.0080
15.7480	17.7165	-0.0022	-0.0037	-0.0018	-0.0043	-0.0044	-0.0060	-0.0041	-0.0065	-0.0050	-0.0088
17.7165	19.6850	-0.0022	-0.0037	-0.0018	-0.0043	-0.0047	-0.0063	-0.0043	-0.0068	-0.0052	-0.0090

ISO Tolerances for Shafts – inch									
Diameter in		Deviations in							
		a10		a11		a12		a13	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
–	0.1181	-0.0106	-0.0122	-0.0106	-0.0130	-0.0106	-0.0146	-0.0106	-0.0161
0.1181	0.2362	-0.0106	-0.0125	-0.0106	-0.0136	-0.0106	-0.0154	-0.0106	-0.0177
0.2362	0.3937	-0.0110	-0.0133	-0.0110	-0.0146	-0.0110	-0.0169	-0.0110	-0.0197
0.3937	0.7087	-0.0114	-0.0142	-0.0114	-0.0157	-0.0114	-0.0185	-0.0114	-0.0220
0.7087	1.1811	-0.0118	-0.0151	-0.0118	-0.0169	-0.0118	-0.0201	-0.0118	-0.0248
1.1811	1.5748	-0.0122	-0.0161	-0.0122	-0.0185	-0.0122	-0.0220	-0.0122	-0.0276
1.5748	1.9685	-0.0126	-0.0165	-0.0126	-0.0189	-0.0126	-0.0224	-0.0126	-0.0280
1.9685	2.5591	-0.0134	-0.0181	-0.0134	-0.0209	-0.0134	-0.0252	-0.0134	-0.0315
2.5591	3.1496	-0.0142	-0.0189	-0.0142	-0.0217	-0.0142	-0.0260	-0.0142	-0.0323
3.1496	3.9370	-0.0150	-0.0205	-0.0150	-0.0236	-0.0150	-0.0287	-0.0150	-0.0362
3.9370	4.7244	-0.0161	-0.0217	-0.0161	-0.0248	-0.0161	-0.0299	-0.0161	-0.0374
4.7244	5.5118	-0.0181	-0.0244	-0.0181	-0.0280	-0.0181	-0.0339	-0.0181	-0.0429
5.5118	6.2992	-0.0205	-0.0268	-0.0205	-0.0303	-0.0205	-0.0362	-0.0205	-0.0453
6.2992	7.0866	-0.0228	-0.0291	-0.0228	-0.0327	-0.0228	-0.0386	-0.0228	-0.0476
7.0866	7.8740	-0.0260	-0.0333	-0.0260	-0.0374	-0.0260	-0.0441	-0.0260	-0.0543
7.8740	8.8583	-0.0291	-0.0364	-0.0291	-0.0406	-0.0291	-0.0472	-0.0291	-0.0575
8.8583	9.8425	-0.0323	-0.0396	-0.0323	-0.0437	-0.0323	-0.0504	-0.0323	-0.0606
9.8425	11.0236	-0.0362	-0.0445	-0.0362	-0.0488	-0.0362	-0.0567	-0.0362	-0.0681
11.0236	12.4016	-0.0413	-0.0496	-0.0413	-0.0539	-0.0413	-0.0618	-0.0413	-0.0732
12.4016	13.9764	-0.0472	-0.0563	-0.0472	-0.0614	-0.0472	-0.0697	-0.0472	-0.0823
13.9764	15.7480	-0.0531	-0.0622	-0.0531	-0.0673	-0.0531	-0.0756	-0.0531	-0.0882

Diameter in		Deviations in						Deviations in					
		c11		c12		c13		e11		e12		e13	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	0.1181	-0.0024	-0.0047	-0.0024	-0.0063	-0.0024	-0.0079	-0.0006	-0.0029	-0.0006	-0.0045	-0.0006	-0.0061
0.1181	0.2362	-0.0028	-0.0057	-0.0028	-0.0075	-0.0028	-0.0098	-0.0008	-0.0037	-0.0008	-0.0055	-0.0008	-0.0079
0.2362	0.3937	-0.0031	-0.0067	-0.0031	-0.0091	-0.0031	-0.0118	-0.0010	-0.0045	-0.0010	-0.0069	-0.0010	-0.0096
0.3937	0.7087	-0.0037	-0.0081	-0.0037	-0.0108	-0.0037	-0.0144	-0.0013	-0.0056	-0.0013	-0.0083	-0.0013	-0.0119
0.7087	1.1811	-0.0043	-0.0094	-0.0043	-0.0126	-0.0043	-0.0173	-0.0016	-0.0067	-0.0016	-0.0098	-0.0016	-0.0146
1.1811	1.5748	-0.0047	-0.0110	-0.0047	-0.0146	-0.0047	-0.0201	-0.0020	-0.0083	-0.0020	-0.0118	-0.0020	-0.0173
1.5748	1.9685	-0.0051	-0.0114	-0.0051	-0.0150	-0.0051	-0.0205	-0.0020	-0.0083	-0.0020	-0.0118	-0.0020	-0.0173
1.9685	2.5591	-0.0055	-0.0130	-0.0055	-0.0173	-0.0055	-0.0236	-0.0024	-0.0098	-0.0024	-0.0142	-0.0024	-0.0205
2.5591	3.1496	-0.0059	-0.0134	-0.0059	-0.0177	-0.0059	-0.0240	-0.0024	-0.0098	-0.0024	-0.0142	-0.0024	-0.0205
3.1496	3.9370	-0.0067	-0.0154	-0.0067	-0.0205	-0.0067	-0.0280	-0.0028	-0.0115	-0.0028	-0.0166	-0.0028	-0.0241
3.9370	4.7244	-0.0071	-0.0157	-0.0071	-0.0209	-0.0071	-0.0283	-0.0028	-0.0115	-0.0028	-0.0166	-0.0028	-0.0241
4.7244	5.5118	-0.0079	-0.0177	-0.0079	-0.0236	-0.0079	-0.0327	-0.0033	-0.0132	-0.0033	-0.0191	-0.0033	-0.0281
5.5118	6.2992	-0.0083	-0.0181	-0.0083	-0.0240	-0.0083	-0.0331	-0.0033	-0.0132	-0.0033	-0.0191	-0.0033	-0.0281
6.2992	7.0866	-0.0091	-0.0189	-0.0091	-0.0248	-0.0091	-0.0339	-0.0033	-0.0132	-0.0033	-0.0191	-0.0033	-0.0281
7.0866	7.8740	-0.0094	-0.0209	-0.0094	-0.0276	-0.0094	-0.0378	-0.0039	-0.0154	-0.0039	-0.0220	-0.0039	-0.0323
7.8740	8.8583	-0.0102	-0.0217	-0.0102	-0.0283	-0.0102	-0.0386	-0.0039	-0.0154	-0.0039	-0.0220	-0.0039	-0.0323
8.8583	9.8425	-0.0110	-0.0224	-0.0110	-0.0291	-0.0110	-0.0394	-0.0039	-0.0154	-0.0039	-0.0220	-0.0039	-0.0323
9.8425	11.0236	-0.0118	-0.0244	-0.0118	-0.0323	-0.0118	-0.0437	-0.0043	-0.0169	-0.0043	-0.0248	-0.0043	-0.0362
11.0236	12.4016	-0.0130	-0.0256	-0.0130	-0.0335	-0.0130	-0.0449	-0.0043	-0.0169	-0.0043	-0.0248	-0.0043	-0.0362
12.4016	13.9764	-0.0142	-0.0283	-0.0142	-0.0366	-0.0142	-0.0492	-0.0049	-0.0191	-0.0049	-0.0274	-0.0049	-0.0400
13.9764	15.7480	-0.0157	-0.0299	-0.0157	-0.0382	-0.0157	-0.0508	-0.0049	-0.0191	-0.0049	-0.0274	-0.0049	-0.0400

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ENGINEERING

ISO Tolerances for Shafts – inch

Diameter in		Deviations in						Deviations in					
		f5		f6		f7		g5		g6		g7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	0.1181	-0.0002	-0.0004	-0.0002	-0.0005	-0.0002	-0.0006	-0.0001	-0.0002	-0.0001	-0.0003	-0.0001	-0.0005
0.1181	0.2362	-0.0004	-0.0006	-0.0004	-0.0007	-0.0004	-0.0009	-0.0002	-0.0004	-0.0002	-0.0005	-0.0002	-0.0006
0.2362	0.3937	-0.0005	-0.0007	-0.0005	-0.0009	-0.0005	-0.0011	-0.0002	-0.0004	-0.0002	-0.0006	-0.0002	-0.0008
0.3937	0.7087	-0.0006	-0.0009	-0.0006	-0.0011	-0.0006	-0.0013	-0.0002	-0.0006	-0.0002	-0.0007	-0.0002	-0.0009
0.7087	1.1811	-0.0008	-0.0011	-0.0008	-0.0013	-0.0008	-0.0016	-0.0003	-0.0006	-0.0003	-0.0008	-0.0003	-0.0011
1.1811	1.9685	-0.0010	-0.0014	-0.0010	-0.0016	-0.0010	-0.0020	-0.0004	-0.0008	-0.0004	-0.0010	-0.0004	-0.0013
1.9685	3.1496	-0.0012	-0.0017	-0.0012	-0.0019	-0.0012	-0.0024	-0.0004	-0.0009	-0.0004	-0.0011	-0.0004	-0.0016
3.1496	4.7244	-0.0014	-0.0020	-0.0014	-0.0023	-0.0014	-0.0028	-0.0005	-0.0011	-0.0005	-0.0013	-0.0005	-0.0019
4.7244	7.0866	-0.0017	-0.0024	-0.0017	-0.0027	-0.0017	-0.0033	-0.0006	-0.0013	-0.0006	-0.0015	-0.0006	-0.0021
7.0866	9.8425	-0.0020	-0.0028	-0.0020	-0.0031	-0.0020	-0.0038	-0.0006	-0.0014	-0.0006	-0.0017	-0.0006	-0.0024
9.8425	12.4016	-0.0022	-0.0031	-0.0022	-0.0035	-0.0022	-0.0043	-0.0007	-0.0016	-0.0007	-0.0019	-0.0007	-0.0027
12.4016	15.7480	-0.0024	-0.0034	-0.0024	-0.0039	-0.0024	-0.0047	-0.0007	-0.0017	-0.0007	-0.0021	-0.0007	-0.0030

Diameter in		Deviations in									
		h4		h5		h6		h7		h8	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	0.1181	0	-0.00012	0	-0.00016	0	-0.00024	0	-0.0004	0	-0.0006
0.1181	0.2362	0	-0.00016	0	-0.00020	0	-0.00031	0	-0.0005	0	-0.0007
0.2362	0.3937	0	-0.0002	0	-0.00024	0	-0.0004	0	-0.0006	0	-0.0009
0.3937	0.7087	0	-0.0002	0	-0.00031	0	-0.0004	0	-0.0007	0	-0.0011
0.7087	1.1811	0	-0.0002	0	-0.0004	0	-0.0005	0	-0.0008	0	-0.0013
1.1811	1.9685	0	-0.0003	0	-0.0004	0	-0.0006	0	-0.0010	0	-0.0015
1.9685	3.1496	0	-0.0003	0	-0.0005	0	-0.0007	0	-0.0012	0	-0.0018
3.1496	4.7244	0	-0.0004	0	-0.0006	0	-0.0009	0	-0.0014	0	-0.0021
4.7244	7.0866	0	-0.0005	0	-0.0007	0	-0.0010	0	-0.0016	0	-0.0025
7.0866	9.8425	0	-0.0006	0	-0.0008	0	-0.0011	0	-0.0018	0	-0.0028
9.8425	12.4016	0	-0.0006	0	-0.0009	0	-0.0013	0	-0.0020	0	-0.0032
12.4016	15.7480	0	-0.0007	0	-0.0010	0	-0.0014	0	-0.0022	0	-0.0035

Diameter in		Deviations in									
		h9		h10		h11		h12		h13	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	0.1181	0	-0.0010	0	-0.0016	0	-0.0024	0	-0.0039	0	-0.0055
0.1181	0.2362	0	-0.0012	0	-0.0019	0	-0.0030	0	-0.0047	0	-0.0071
0.2362	0.3937	0	-0.0014	0	-0.0023	0	-0.0035	0	-0.0059	0	-0.0087
0.3937	0.7087	0	-0.0017	0	-0.0028	0	-0.0043	0	-0.0071	0	-0.0106
0.7087	1.1811	0	-0.0020	0	-0.0033	0	-0.0051	0	-0.0083	0	-0.0130
1.1811	1.9685	0	-0.0024	0	-0.0039	0	-0.0063	0	-0.0098	0	-0.0154
1.9685	3.1496	0	-0.0029	0	-0.0047	0	-0.0075	0	-0.0118	0	-0.0181
3.1496	4.7244	0	-0.0034	0	-0.0055	0	-0.0087	0	-0.0138	0	-0.0213
4.7244	7.0866	0	-0.0039	0	-0.0063	0	-0.0098	0	-0.0157	0	-0.0248
7.0866	9.8425	0	-0.0045	0	-0.0073	0	-0.0114	0	-0.0181	0	-0.0283
9.8425	12.4016	0	-0.0051	0	-0.0083	0	-0.0126	0	-0.0205	0	-0.0319
12.4016	15.7480	0	-0.0055	0	-0.0091	0	-0.0142	0	-0.0224	0	-0.0350

ISO Tolerances for Shafts – inch

Diameter in		Deviations in						Deviations in					
		j5		j6		j7		k5		k6		k7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	0.1181	+0.00008	-0.00008	+0.00016	-0.00008	+0.00024	-0.00016	+0.00016	0	+0.00024	0	+0.00039	0
0.1181	0.2362	+0.00012	-0.00008	+0.00024	-0.00008	+0.00031	-0.00016	+0.00024	+0.00004	+0.00035	+0.00004	+0.00051	+0.00004
0.2362	0.3937	+0.00016	-0.00008	+0.00028	-0.00008	+0.00039	-0.00020	+0.00028	+0.00004	+0.00039	+0.00004	+0.00063	+0.00004
0.3937	0.7087	+0.00020	-0.00012	+0.00031	-0.00012	+0.00047	-0.00024	+0.00035	+0.00004	+0.00047	+0.00004	+0.00075	+0.00004
0.7087	1.1811	+0.00020	-0.00016	+0.00035	-0.00016	+0.00051	-0.00031	+0.00043	+0.00008	+0.00059	+0.00008	+0.00091	+0.00008
1.1811	1.9685	+0.00024	-0.00020	+0.00043	-0.00020	+0.00059	-0.00039	+0.00051	+0.00008	+0.00071	+0.00008	+0.00106	+0.00008
1.9685	3.1496	+0.00024	-0.00028	+0.00047	-0.00028	+0.00071	-0.00047	+0.00059	+0.00008	+0.00083	+0.00008	+0.00126	+0.00008
3.1496	4.7244	+0.00024	-0.00035	+0.00051	-0.00035	+0.00079	-0.00059	+0.00071	+0.00012	+0.00098	+0.00012	+0.00150	+0.00012
4.7244	7.0866	+0.00028	-0.00043	+0.00055	-0.00043	+0.00087	-0.00071	+0.00083	+0.00012	+0.00110	+0.00012	+0.00169	+0.00012
7.0866	9.8425	+0.00028	-0.00051	+0.00063	-0.00051	+0.00098	-0.00083	+0.00094	+0.00016	+0.00130	+0.00016	+0.00197	+0.00016
9.8425	12.4016	+0.00028	-0.00063	+0.00063	-0.00063	+0.00102	-0.00102	+0.00106	+0.00016	+0.00142	+0.00016	+0.00220	+0.00016
12.4016	15.7480	+0.00028	-0.00071	+0.00071	-0.00071	+0.00114	-0.00110	+0.00114	+0.00016	+0.00157	+0.00016	+0.00240	+0.00016

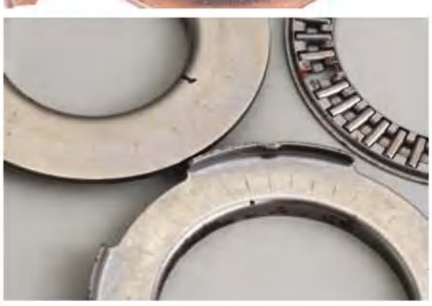
Diameter in		Deviations in						Deviations in					
		m5		m6		m7		n5		n6		n7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
—	0.1181	+0.00024	+0.00008	+0.00031	+0.00008	+0.00047	+0.00008	+0.0003	+0.0002	+0.0004	+0.0002	+0.0006	+0.0002
0.1181	0.2362	+0.00035	+0.00016	+0.00047	+0.00016	+0.00063	+0.00016	+0.0005	+0.0003	+0.0006	+0.0003	+0.0008	+0.0003
0.2362	0.3937	+0.00047	+0.00024	+0.00059	+0.00024	+0.00083	+0.00024	+0.0006	+0.0004	+0.0007	+0.0004	+0.0010	+0.0004
0.3937	0.7087	+0.00059	+0.00028	+0.00071	+0.00028	+0.00098	+0.00028	+0.0008	+0.0005	+0.0009	+0.0005	+0.0012	+0.0005
0.7087	1.1811	+0.00067	+0.00031	+0.00083	+0.00031	+0.00114	+0.00031	+0.0009	+0.0006	+0.0011	+0.0006	+0.0014	+0.0006
1.1811	1.9685	+0.00079	+0.00035	+0.00098	+0.00035	+0.00134	+0.00035	+0.0011	+0.0007	+0.0013	+0.0007	+0.0017	+0.0007
1.9685	3.1496	+0.00094	+0.00043	+0.00118	+0.00043	+0.00161	+0.00043	+0.0013	+0.0008	+0.0015	+0.0008	+0.0020	+0.0008
3.1496	4.7244	+0.00110	+0.00051	+0.00138	+0.00051	+0.00189	+0.00051	+0.0015	+0.0009	+0.0018	+0.0009	+0.0023	+0.0009
4.7244	7.0866	+0.00130	+0.00059	+0.00157	+0.00059	+0.00217	+0.00059	+0.0018	+0.0011	+0.0020	+0.0011	+0.0026	+0.0011
7.0866	9.8425	+0.00146	+0.00067	+0.00181	+0.00067	+0.00248	+0.00067	+0.0020	+0.0012	+0.0024	+0.0012	+0.0030	+0.0012
9.8425	12.4016	+0.00169	+0.00079	+0.00205	+0.00079	+0.00283	+0.00079	+0.0022	+0.0013	+0.0026	+0.0013	+0.0034	+0.0013
12.4016	15.7480	+0.00181	+0.00083	+0.00224	+0.00083	+0.00307	+0.00083	+0.0024	+0.0015	+0.0029	+0.0015	+0.0037	+0.0015

Diameter in		Deviations in					
		p6		r6		r7	
>	≤	Max.	Min.	Max.	Min.	Max.	Min.
3.1496	3.9370	+0.0023	+0.0015	-	-	-	-
3.9370	4.7244	+0.0023	+0.0015	-	-	-	-
4.7244	5.5118	+0.0027	+0.0017	+0.0035	+0.0026	-	-
5.5118	6.2992	+0.0027	+0.0017	+0.0035	+0.0026	-	-
6.2992	7.0866	+0.0027	+0.0017	+0.0035	+0.0026	-	-
7.0866	7.8740	+0.0031	+0.0020	+0.0042	+0.0030	-	-
7.8740	8.8583	+0.0031	+0.0020	+0.0043	+0.0031	+0.0050	+0.0031
8.8583	9.8425	+0.0031	+0.0020	+0.0044	+0.0033	+0.0051	+0.0033
9.8425	11.0236	+0.0035	+0.0022	+0.0050	+0.0037	+0.0057	+0.0037
11.0236	12.4016	+0.0035	+0.0022	+0.0051	+0.0039	+0.0059	+0.0039
12.4016	13.9764	+0.0039	+0.0024	+0.0057	+0.0043	+0.0065	+0.0043
13.9764	15.7480	+0.0039	+0.0024	+0.0059	+0.0045	+0.0067	+0.0045
15.7480	17.7165	+0.0043	+0.0027	+0.0065	+0.0050	+0.0074	+0.0050
17.7165	19.6850	+0.0043	+0.0027	+0.0068	+0.0052	+0.0077	+0.0052

EXAMPLES OF BEARING FAILURES

Failures		Characteristics
(1) Flaking	  	Flaking is a phenomenon that material is removed in flakes from a surface layer of the bearing raceways or rolling elements due to rolling fatigue. This phenomenon is generally attributed to the approaching end of bearing service life. However, if flaking occurs at early stages of bearing service life, it is necessary to determine causes and adopt countermeasures, since there is a possibility of abnormality in this case. Pitting Pitting is another type of failure caused by rolling fatigue, in which minute holes of approx. 0.1 mm in depth are generated on the raceway surface. Peeling (shown in middle figure) Peeling is a phenomenon in which the lubricant film separation is insuffcient for complete surface separation (0.02 mm or less) of the rolling surfaces causing fatigue and peeling due to concentrated stress acting on microscopic peaks of surface roughness.
(2) Cracking Chipping	 	Cracking is mainly triggered by debris initiated defects due to wear of other system components, partial shape defects, and concentrated stress and overload caused by edge load. It may occur on bearing rings due to fatigue caused by repeated bend stress.

	Damages	Causes	Countermeasures
	Flaking occurring at an incipient stage	· Too small internal clearance · Improper or insufficient lubricant · Load too high · Rust	· Provide proper internal clearance. · Select proper lubricating method or lubricant.
	Symmetrical flaking along circumference of raceway	· Inaccurate housing roundness	· Correct processing accuracy of housing bore. Especially for split housings, care should be taken to ensure processing accuracy.
	Flaking occurring near the edge of the raceway or rolling contact surface	· Improper mounting · Shaft deflection · Inaccuracy of the shaft and housing	· Correct centering. · Correct squareness of shaft or housing shoulder.
	Flaking on the raceway surface at the same interval as rolling element spacing	· Heavy impact load during mounting · A flaw caused during mounting · Rust generated while out of operation	· Improve mounting procedure. · Provide rust prevention treatment before long cessation of operation.
	Cracking in outer ring, inner ring or race	· Excessive interference · Excessive fillet on shaft or housing · Heavy impact load · Advanced flaking or seizure · Impact on race during mounting	· Select proper fit. · Adjust fillet in the shaft or in the housing to smaller than that of the bearing chamfer dimension. · Re-examine load conditions. · Improve mounting procedures.
	Cracking on rolling elements	· Heavy impact load · Advanced flaking	· Improve mounting and handling procedures. · Re-examine load conditions.

Failures		Characteristics
(3) Brinelling Nicks		· Brinelling is a small surface indentation generated either on the raceway through plastic deformation at the contact point between the raceway and rolling elements, or on the rolling surfaces from insertion of foreign matter, when heavy load is applied while the bearing is stationary or rotating at a low rotation speed. · Nicks are indentations produced directly by rough handling such as hammering.
(4) Wear		Normally, wear of bearing is observed on sliding contact surfaces such as roller end faces and rib faces, cage pockets, the guide surface of cages and cage riding lands. Wear is not directly related to material fatigue. Wear caused by foreign matter and corrosion can affect not only sliding surfaces but rolling surfaces.
(5) Fretting	 	Fretting occurs to bearings which are subject to vibration while in stationary condition or which are exposed to minute vibrations. It is characterized by rust-colored wear particles. Since fretting on the raceways often appears similar to brinelling, it is sometimes called "false brinelling".
(6) Creeping		Creeping is a phenomenon in which bearing rings move relative to the shaft or housing during operation.

Damages	Causes	Countermeasures
Brinelling on the raceway or rolling contact surface	· Entry of foreign matter	· Clean bearing and its peripheral parts. · Improve sealing devices.
Brinelling on the raceway surface at the same interval as the rolling element spacing	· Impact load during mounting · Excessive load applied while bearing is stationary	· Improve mounting procedure. · Improve machine handling.
Nicks on the raceway or rolling contact surface	· Careless handling	· Improve mounting and handling procedure.
Wear on the contact surfaces (cage pockets, cage riding land)	· Improper or insufficient lubricant	· Select proper lubricating method or lubricant. · Improve sealing device. · Clean the bearing and its peripheral parts.
Wear on raceways and rolling contact surfaces	· Entry of foreign matter · Improper or insufficient lubricant	
Rust-colored wear particles generated on the fitting surface (fretting corrosion)	· Insufficient interference	· Provide greater interference. · Apply lubricant to the fitting surface.
Brinelling on the raceway surface at the same interval as rolling element spacing (false brinelling)	· Vibration and oscillation when bearings are stationary.	· Improve fixing method of the shaft and housing.
Wear, discoloration, and scuffing caused by slipping on the fitting surfaces	· Insufficient interference · Insufficient tightening of sleeve	· Provide greater interference. · Proper tightening of sleeve.

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Failures	Characteristics	
(7) Damage to Cages	 	Since cages are made of low hardness materials, external pressure and contact with other parts can easily produce flaws and distortion. In some cases, these are aggravated and become chips and cracks. Large chips and cracks are often accompanied by deformation, which may reduce the accuracy of the cage itself and may hinder the smooth movement of rolling elements.
(8) Seizing	 	A phenomenon caused by abnormal heating in bearings due to various reasons

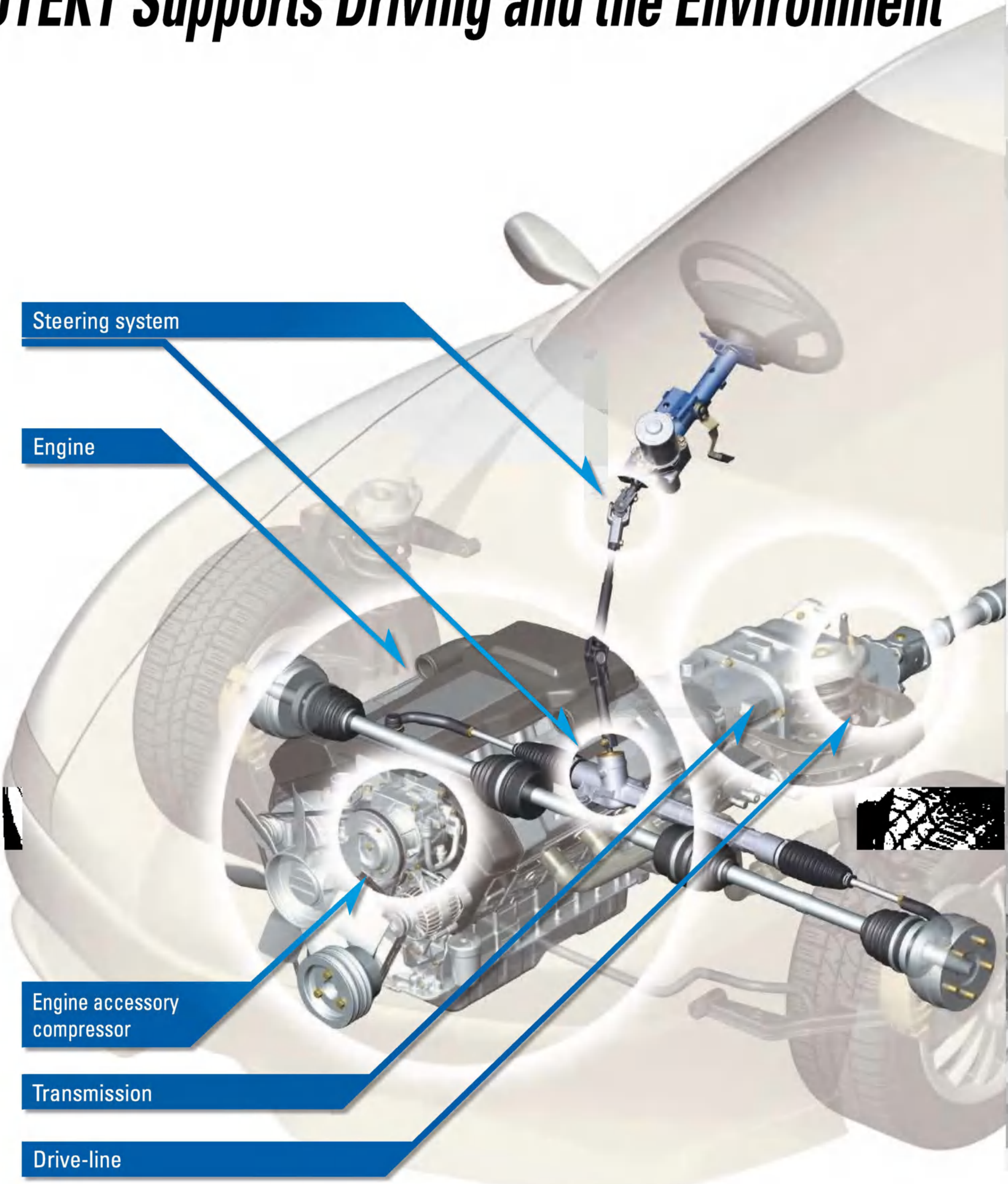
	Damages	Causes	Countermeasures
	Flaws, distortion, chipping, cracking and excessive wear in cages.	· Extraordinary vibration, impact, moment · Improper or insufficient lubricant · Dents made during mounting	· Re-examine load conditions. · Select proper lubricating method or lubricant. · Re-examine cage types. · Improve mounting.
	Discoloration, distortion, and melting together due to heating in bearings	· Too small internal clearance · Improper or insufficient lubricant · Excessive load · Aggravated by other bearing flaws	· Provide proper internal clearance. · Select proper lubricating method or lubricant. · Re-examine bearing type. · Earlier discovery of bearing flaws

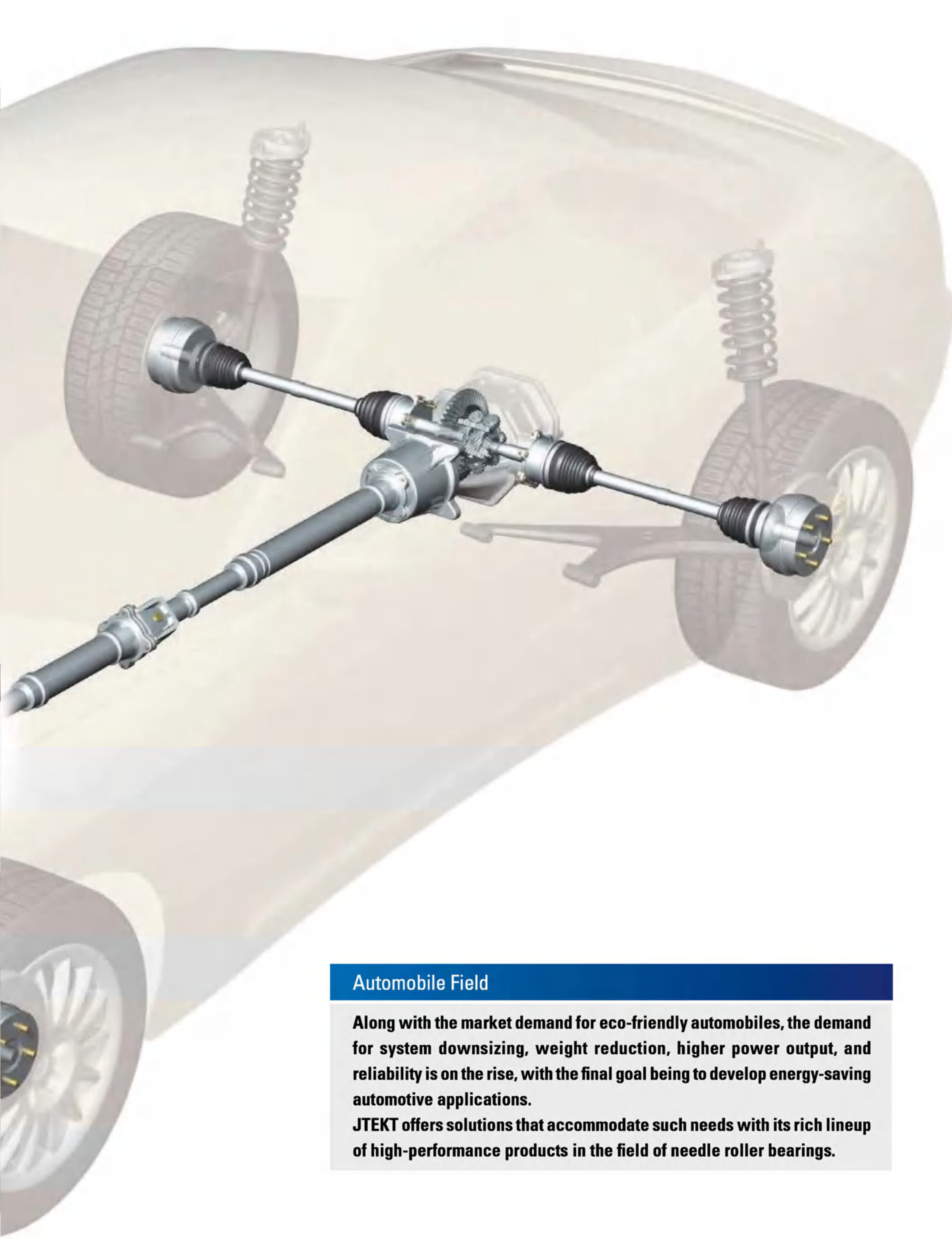
NOTES

APPLICATIONS

NEEDLE ROLLER BEARING APPLICATIONS

JTEKT Supports Driving and the Environment





Automobile Field

Along with the market demand for eco-friendly automobiles, the demand for system downsizing, weight reduction, higher power output, and reliability is on the rise, with the final goal being to develop energy-saving automotive applications.
JTEKT offers solutions that accommodate such needs with its rich lineup of high-performance products in the field of needle roller bearings.

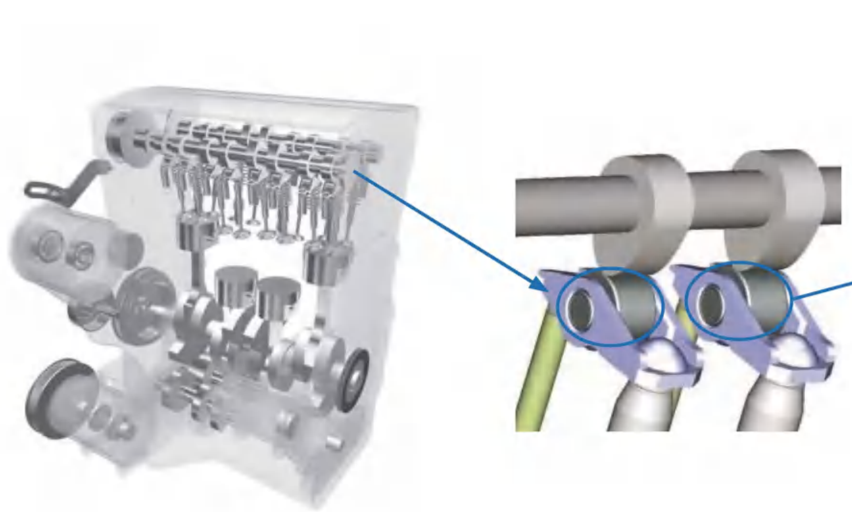
ENGINE

Valve Train Components

JTEKT's needle roller bearings for rocker arms contribute to reductions in energy used by engines and to improvements in engine reliability.

Bearing Features

- Low torque
- Wear resistance



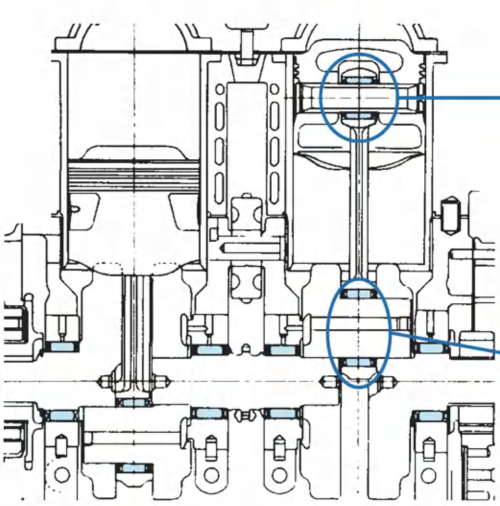
Roller finger follower assemblies

Piston and Crank Components

JTEKT's needle roller bearings for connecting rod applications respond to the need for reductions in energy used by engines and to demanding lubrication requirements, contributing to greater reliability.

Bearing Features

- Durability
- Improvement in seizure resistance
- Supports higher loads



Engines for motorcycles and boats

Radial needle roller and cage assemblies

Balance Shaft Components

JTEKT's needle roller bearings for balance shafts contribute to improved lubrication methods, reduced friction, and improved reliability under vibration conditions.

Bearing Features

- High reliability
- Vibration resistance

Heavy-duty needle roller bearings

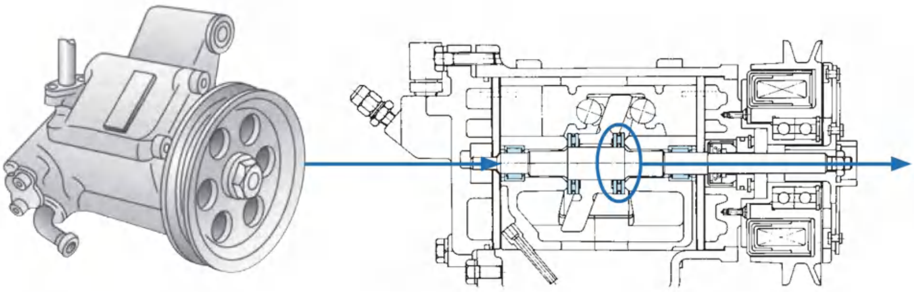
ENGINE ACCESSORIES

Compressor Components

JTEKT's needle roller bearings for compressors contribute to support for thin film lubricants, improved efficiency, and improved reliability.

Bearing Features

- Wear resistance
- Low torque
- Improved lubricity



Thrust bearings

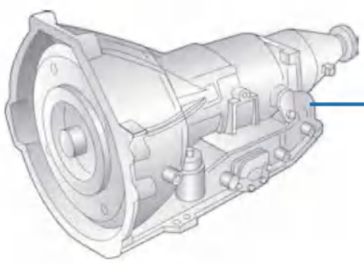
TRANSMISSION

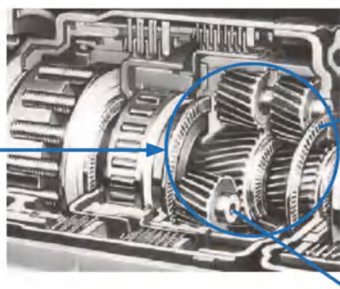
JTEKT's needle roller bearings for transmissions contribute to reductions in the size and weight of the transmission, improved power and fuel efficiency, support for low-viscosity lubricants, and improved reliability.

Bearing Features

- Supports higher loads
- Longer life in oil with foreign material
- Low torque

Automatic Transmissions

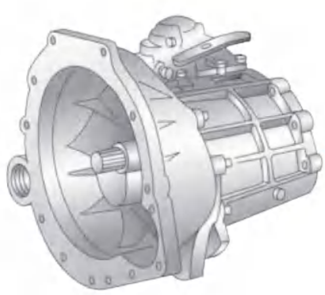


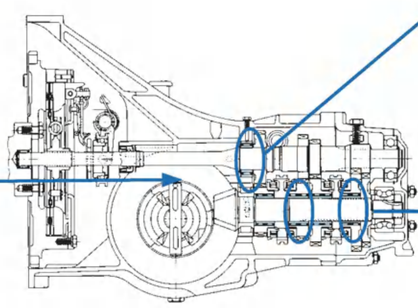


Thrust bearings

Radial needle roller and cage assemblies

Manual Transmissions





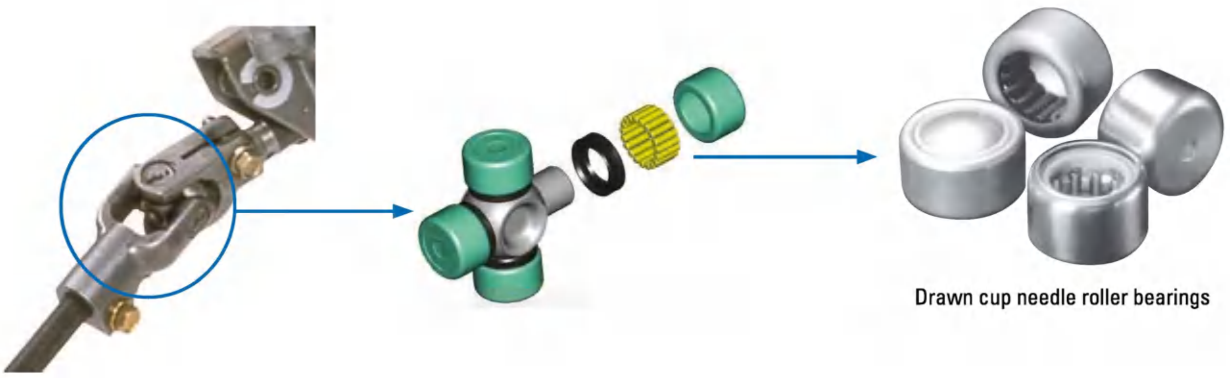
Split polymer caged radial assemblies

STEERING SYSTEMS

JTEKT's needle roller bearings for steering systems realize smooth steering capability with high reliability and quiet running by drawing on our experience in producing safe steering system components.

Bearing Features
- High reliability
- Reduced noise
- High rigidity

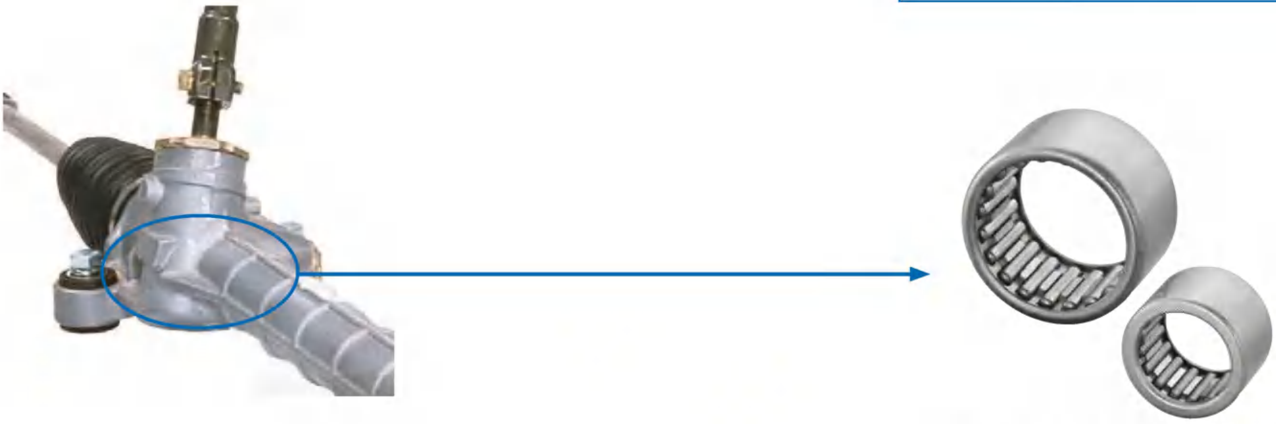
Intermediate Steering Shafts



Drawn cup needle roller bearings

Pinion Shafts

Bearing Features
- High reliability
- Reduced noise



Drawn cup needle roller bearings

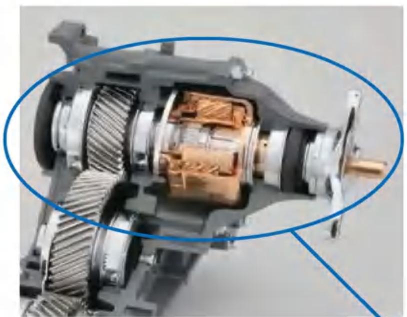
DRIVE-LINES

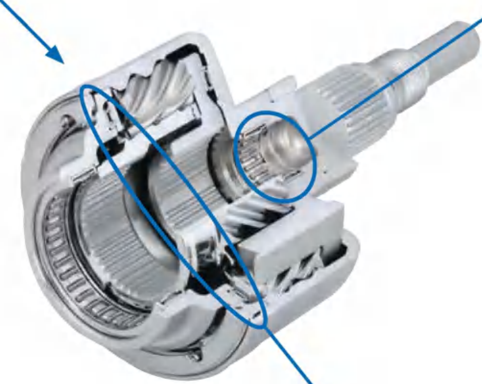
Torque Sensing LSD

JTEKT's needle roller bearings for torque sensing LSDs contribute to downsizing and weight reduction, higher efficiency, and improved reliability.

Bearing Features

- Alleviates misalignment
- Supports higher loads





Drawn cup needle roller bearings

Thrust bearings

INDUSTRIAL MACHINERY FIELD

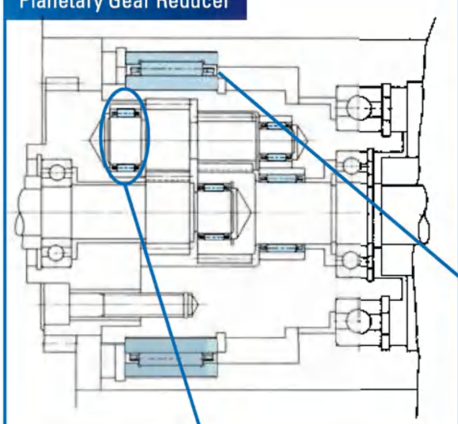
Construction equipment and agricultural machinery are used in dimanding environments and therefore require high durability. JTEKT offers high-performance needle roller bearings that respond to energy-saving requirements and high reliability needs.

Construction Equipment

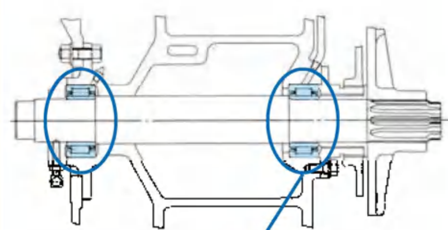
Bearing Features

- High reliability

Planetary Gear Reducer



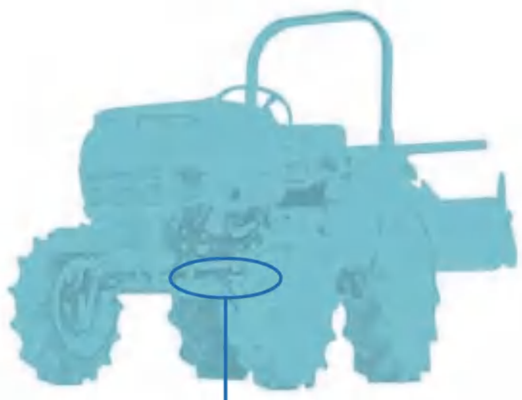
Wheel Drum



Radial needle roller and cage assemblies

Heavy-duty needle roller bearings

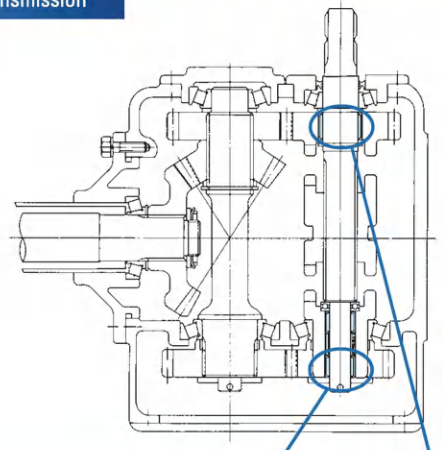
Agricultural Machinery



Bearing Features

- High reliability

Transmission

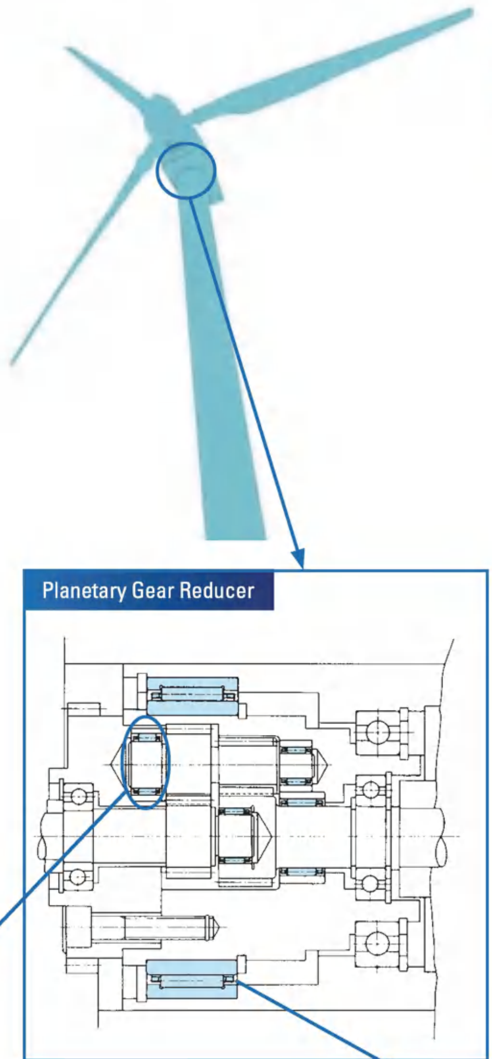


Radial needle roller and cage assemblies

WIND POWER GENERATION

Bearings used in wind power generators require long service lives.
JTEKT offers high-performance needle roller bearings that support high reliability and demanding environmental conditions.

Wind Power Generation



Bearing Features

- Long service life
- Reduced noise

Radial needle roller and cage assemblies

Heavy-duty needle roller bearings

NOTES